



SITE ID: 095-01-b9ecb

SITE ADDRESS: 928 JAMES HAYES RD.,
DEEP GAP, NC 28618

North Carolina Emergency Management – Private Roads and Bridges

Site Information Form

Site Number: 095-01-b9ecb

Site Address: 928 James Hayes Road, Deep Gap, NC 28618

GPS Coordinates: 36.19958, -81.57724

County: Watauga

Bridge Type: Steel I-beam with Timber Decking or Modular Steel Bridge

Span Length: 30 ft Standard Bridge or 40 ft Modular Bridge. Refer to BSR for required waterway opening.

Bridge Width: 12'-0" Clear Width

Substructure Type: Concrete Cap on Drilled-in Piles

Geotechnical Information: See Standard Bridge Plans or the Modular Bridge Substructure Plans for Notes

Additional Notes: _____

Timber bridge railing not required for Steel I-beam with timber decking option.

Modular Steel Bridge option shall include guardrail as part of the system.

Wingwalls are not required.

The existing bridge is in place and must be removed by the Contractor prior to the start of construction.

No known debris or obstructions in the stream requiring removal.

NC DEPARTMENT OF EMERGENCY MANAGEMENT
PRIVATE ROADS AND BRIDGES PROGRAM

This certification demonstrates that the newly designed and installed private bridge/culvert provides conveyance greater than or equal to the original destroyed crossing. This is based on the best available data provided from post storm evaluations. Portions of the existing structures may have been destroyed, removed, modified or shifted from their original location or elevation.



Johnson, Mirmiran, & Thompson Inc.
 108 Asheville Commerce Parkway
 Candler, NC, 28715
 License No: C-3097

BSR based on STANDARD BRIDGE PLANS

BRIDGE SURVEY & HYDRAULIC DESIGN REPORT

NC DEPARTMENT OF EMERGENCY MANAGEMENT
PRIVATE ROADS AND BRIDGES PROGRAM

Site Number

095-01-b9ecb

Latitude

36.19958

Longitude

-81.57724

County

Watauga

Address

near 928 James Hayes Road

City

Deep Gap, NC

Zip Code

28618

Recommended Structure

1 @ 40' Steel Modular Bridge (30' effective flow length)

Recommended Width of Roadway

Skew

Recommended Location is

(A) Upstream, Downstream) of Existing Crossing

Temporary Crossing



I hereby certify that that I have reviewed the existing hydraulic conveyance at this site which was approximately a 25 ft timber bridge with the proposed conveyance provided by the proposed 40 ft. span bridge.

The proposed bridge low chord for the bridge shall be set in accordance with the the FEMA Disaster Specific Guidance for the Replacement of Private Roads and Bridges issued on 14 February 2025, "to provide bridge/culvert design plans certified (sealed, signed, and dated) by a Professional Engineer licensed in the State of North Carolina demonstrating that the newly designed and installed private bridge/culvert provides conveyance greater than or equal to the original destroyed crossing".

This certification demonstrates that the newly designed and installed private bridge/culvert provides conveyance greater than or equal to the original destroyed crossing. This is based on the best available data provided from post storm evaluations. Portions of the existing structures may have been destroyed, removed, modified or shifted from their original location or elevation.

Designed by

Assisted by

Date

Seal

Professional Engineer

Matthew D. Foster

781932BFAFC8472...

Signed by:

Matthew D Foster

7/27/2026

12:28:00 PM EDT

Reviewed by

Date

Initial

MDF

SITE DATA

Drainage Area

Source

River Basin

Yadkin - PeeDee

Character

Stream Classification (e.g., Trout, High Quality Water)

B; Tr, ORW

Debris Potential: Low

Moderate

High

Existing Structure - Source of Available Data

NCEM Private Roads and Bridges Inspection Team

Existing Structure - Description

1 @ 25 ft. +/- timber bridge

Estimated Waterway Opening

86.8

ft²

Design Control Elev

ft

Source

Gage Station No

Period of Records

Max Discharge

cfs

Date

Frequency

Historical Flood Information:

Date

Elev

ft

Est Freq

yr

Source

Period of Knowledge

yrs

Historical Scour Info: General

ft

Contraction

ft

Local

ft

Channel Slope

ft/ft

Source

Normal Water Surface Elev

ft

Manning's n: Left OB

Channel

Right OB

Source

Flood Study / Status

N/A, Trout Creek is a Tributary to Elk Creek, LDS

Flood Study

With

Without

100-yr Discharge

cfs

WS Elev: Floodway

ft

Floodway

ft

River Station

DESIGN DATA

Hydrological Method

Disaster Specific Guidance for the Replacement of Private Roads and Bridges 2/14/2025

Floods Evaluated

Frequency (year)

Discharge (cfs)

Elevation (ft)

Backwater (ft)

Bridge Opening Velocity (fps)

Waterway Opening Provided Below: Design WS Elev

sf

100-yr WS Elev

sf

Total

113.0

sf

Average Channel Velocity (Design)

fps

Average Overbank Velocity (Design)

fps

Computed Scour: General

ft

Contraction

ft

Local

ft

INFORMATION TO BE SHOWN ON PLANS

HYDRAULIC DATA

DESIGN DISCHARGE

= 260

C.F.S.

FREQUENCY OF DESIGN FLOOD

= 25

YRS.

DESIGN HIGH WATER ELEVATION

=

DRAINAGE AREA

= 0.94

SQ. MI.

BASIC DISCHARGE (Q100)

= 420

C.F.S.

BASIC HIGH WATER ELEVATION

=

OVERTOPPING FLOOD DATA

OVERTOPPING DISCHARGE

=

C.F.S.

FREQUENCY OF OVERTOPPING FLOOD

=

YRS.

OVERTOPPING FLOOD ELEVATION

=

"

*NOTE LOCATION OF OVERTOPPING

WS EL. Taken @ River Station ?

ADDITIONAL INFORMATION AND COMPUTATIONS

Number of Homes Confirmed	Yes
Number of Homes	5
Churches Confirmed	Yes
Number of Churches	0
Schools Confirmed	Yes
Number of Schools	0
Recreational/Business Areas Confirmed	Yes
Number of Recreational/Business Areas	0
General Description	Note same road has site 095-01-9347b farther down for 3 of the same houses. Ridge needs new upstream support beam and bridge is warping.
Overall Condition	Intact
Condition Other	
Site Repair Status	No Repair
Condition Description	Needs repair for cracked support beams. Still holding due to rock under beam.
Expected Level of Effort	Repair
Other Level of Effort	
Horizontal Curve	No
Number of Travel Lanes (LOS)	1
Inclination	No
Roadway Divider	No
Road/Bridge Width (ft)	12.00
Span/Cap Estimate (ft)	25.00
Surface to Water (ft)	6.00
Utility/Mechanical	No
Utility Types	
Pipe Needs Sizing	No
Depth of Pipe	
Geotechnical	Erosion/scour
Other Geotechnical	

12" W12X22 beam
+ 0.25" Steel Plate
+ 0.25" Steel Plate
=12.5" (1'-1/2") ft structure depth)

Proposed Conveyance Area has been reduced by 0.9 sf to account for blockage created by 3 Plank Connectors as shown in Detail A of the Typical Section.

10+00 10+05 10+10 10+15 10+20 10+25 10+30 10+35 10+40 10+45 10+50 10+55 10+60 10+65 10+70

Stationing and elevations shown are relative to the site. Based on an assumed datum. No survey grade field work was performed.

BSR based on MODULAR BRIDGE PLANS

REFERENCE: N/A

PROJECT: N/A

STATE	STATE PROJECT REFERENCE NO.	SHEET NO.	TOTAL SHEETS
N.C.	095-01-b9ecb	1	

STATE OF NORTH CAROLINA
DEPARTMENT OF TRANSPORTATION
DIVISION OF HIGHWAYS
GEOTECHNICAL ENGINEERING UNIT

STRUCTURE
SUBSURFACE INVESTIGATION

COUNTY WATAUGA

PROJECT DESCRIPTION NORTH CAROLINA EMERGENCY
MANAGEMENT-PRIVATE ROADS, BRIDGE REPAIR
AND REPLACEMENT PROGRAM

SITE DESCRIPTION 928 JAMES HAYES ROAD FOR
BRIDGE OVER TROUT CREEK

CONTENTS

<u>SHEET NO.</u>	<u>DESCRIPTION</u>
1	TITLE SHEET
2, 2A	LEGEND (SOIL & ROCK)
3	SITE PLAN
4	BORE LOG(S)
5-6	SITE PHOTOGRAPH(S)

PERSONNEL

C. BRAKE, G.I.T.

S. DAVIS

TY. BEARD

INVESTIGATED BY F&R, Inc.

DRAWN BY T.T. WALKER

CHECKED BY P. ALTON, P.E.

SUBMITTED BY P. ALTON, P.E.

DATE APRIL 2026

CAUTION NOTICE

THE SUBSURFACE INFORMATION AND THE SUBSURFACE INVESTIGATION ON WHICH IT IS BASED WERE MADE FOR THE PURPOSE OF STUDY, PLANNING AND DESIGN, AND NOT FOR CONSTRUCTION OR PAY PURPOSES.

GENERAL SOIL AND ROCK STRATA DESCRIPTIONS AND INDICATED BOUNDARIES ARE BASED ON A GEOTECHNICAL INTERPRETATION OF ALL AVAILABLE SUBSURFACE DATA AND MAY NOT NECESSARILY REFLECT THE ACTUAL SUBSURFACE CONDITIONS BETWEEN BORINGS OR BETWEEN SAMPLED STRATA WITHIN THE BOREHOLE. THE LABORATORY SAMPLE DATA AND THE IN SITU (IN-PLACE) TEST DATA CAN BE RELIED ON ONLY TO THE DEGREE OF RELIABILITY INHERENT IN THE STANDARD TEST METHOD. THE OBSERVED WATER LEVELS OR SOIL MOISTURE CONDITIONS INDICATED IN THE SUBSURFACE INVESTIGATIONS ARE AS RECORDED AT THE TIME OF THE INVESTIGATION. THESE WATER LEVELS OR SOIL MOISTURE CONDITIONS MAY VARY CONSIDERABLY WITH TIME ACCORDING TO CLIMATIC CONDITIONS INCLUDING TEMPERATURES, PRECIPITATION AND WIND, AS WELL AS OTHER NON-CLIMATIC FACTORS.

THE BIDDER OR CONTRACTOR IS CAUTIONED THAT DETAILS SHOWN ON THE SUBSURFACE PLANS ARE PRELIMINARY ONLY AND IN MANY CASES THE FINAL DESIGN DETAILS ARE DIFFERENT. FOR BIDDING AND CONSTRUCTION PURPOSES, REFER TO THE CONSTRUCTION PLANS AND DOCUMENTS FOR FINAL DESIGN INFORMATION ON THIS PROJECT. THE GEOTECHNICAL ENGINEER DOES NOT WARRANT OR GUARANTEE THE SUFFICIENCY OR ACCURACY OF THE INVESTIGATION MADE, NOR THE INTERPRETATIONS MADE, OR OPINION OF THE GEOTECHNICAL ENGINEER AS TO THE TYPE OF MATERIALS AND CONDITIONS TO BE ENCOUNTERED. THE BIDDER OR CONTRACTOR IS CAUTIONED TO PERFORM INDEPENDENT SUBSURFACE INVESTIGATIONS AND MAKE INTERPRETATIONS AS NECESSARY TO CONFIRM CONDITIONS ENCOUNTERED ON THE PROJECT. THE CONTRACTOR SHALL HAVE NO CLAIM FOR ADDITIONAL COMPENSATION OR FOR AN EXTENSION OF TIME FOR ANY REASON RESULTING FROM THE ACTUAL CONDITIONS ENCOUNTERED AT THE SITE DIFFERING FROM THOSE INDICATED IN THE SUBSURFACE INFORMATION.

NOTES:

1. THE INFORMATION CONTAINED HEREIN IS NOT IMPLIED OR GUARANTEED BY THE GEOTECHNICAL ENGINEER AS ACCURATE NOR IS IT CONSIDERED PART OF THE PLANS, SPECIFICATIONS OR CONTRACT FOR THE PROJECT.
2. BY HAVING REQUESTED THIS INFORMATION, THE CONTRACTOR SPECIFICALLY WAIVES ANY CLAIMS FOR INCREASED COMPENSATION OR EXTENSION OF TIME BASED ON DIFFERENCES BETWEEN THE CONDITIONS INDICATED HEREIN AND THE ACTUAL CONDITIONS AT THE PROJECT SITE.

SINCE



1881

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FROEHLING & ROBERTSON, INC.

Engineering Stability Since 1881

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Raleigh, North Carolina 27603-2302
License No. F-0266
Bus: 919.828.3441 Fax: 919.828.5751



SIGNATURE

DATE

**DOCUMENT NOT CONSIDERED FINAL
UNLESS ALL SIGNATURES COMPLETED**

DRILL UNITS: ☐ CME-45C ☐ CME-55 ☐ CME-550 ☐ VANE SHEAR TEST ☐ PORTABLE HOIST ☒ <u>CME-550X</u> ☐	ADVANCING TOOLS: ☐ CLAY BITS ☐ 6" CONTINUOUS FLIGHT AUGER ☒ 8" HOLLOW AUGERS ☐ HARD FACED FINGER BITS ☐ TUNG-CARBIDE INSERTS ☐ CASING ☐ W/ ADVANCER ☐ TRICONE _____ " STEEL TEETH ☐ TRICONE _____ " TUNG-CARB. ☐ CORE BIT ☐	HAMMER TYPE: ☒ AUTOMATIC ☐ MANUAL CORE SIZE: ☐ -B _____ ☐ -H _____ ☐ -N _____ HAND TOOLS: ☐ POST HOLE DIGGER ☐ HAND AUGER ☐ SOUNDING ROD ☐ VANE SHEAR TEST ☐
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**NORTH CAROLINA DEPARTMENT OF TRANSPORTATION
DIVISION OF HIGHWAYS
GEOTECHNICAL ENGINEERING UNIT**

SUBSURFACE INVESTIGATION

SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS (PAGE 2 OF 2)

ROCK DESCRIPTION

HARD ROCK IS NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT REFUSAL IF TESTED. AN INFERRED ROCK LINE INDICATES THE LEVEL AT WHICH NON-COASTAL PLAIN MATERIAL WOULD YIELD SPT REFUSAL. SPT REFUSAL IS PENETRATION BY A SPLIT SPOON SAMPLER EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS IN NON-COASTAL PLAIN MATERIAL. THE TRANSITION BETWEEN SOIL AND ROCK IS OFTEN REPRESENTED BY A ZONE OF WEATHERED ROCK. ROCK MATERIALS ARE TYPICALLY DIVIDED AS FOLLOWS:

WEATHERED ROCK (WR)		NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT N VALUES > 100 BLOWS PER FOOT IF TESTED.
CRYSTALLINE ROCK (CR)		FINE TO COARSE GRAIN IGNEOUS AND METAMORPHIC ROCK THAT WOULD YIELD SPT REFUSAL IF TESTED. ROCK TYPE INCLUDES GRANITE, GNEISS, GABBRO, SCHIST, ETC.
NON-CRYSTALLINE ROCK (NCR)		FINE TO COARSE GRAIN METAMORPHIC AND NON-COASTAL PLAIN SEDIMENTARY ROCK THAT WOULD YIELD SPT REFUSAL IF TESTED. ROCK TYPE INCLUDES PHYLLITE, SLATE, SANDSTONE, ETC.
COASTAL PLAIN SEDIMENTARY ROCK (CPS)		COASTAL PLAIN SEDIMENTS CEMENTED INTO ROCK, BUT MAY NOT YIELD SPT REFUSAL. ROCK TYPE INCLUDES LIMESTONE, SANDSTONE, CEMENTED SHELL BEDS, ETC.

WEATHERING

FRESH	ROCK FRESH, CRYSTALS BRIGHT, FEW JOINTS MAY SHOW SLIGHT STAINING. ROCK RINGS UNDER HAMMER IF CRYSTALLINE.
VERY SLIGHT (V SL.)	ROCK GENERALLY FRESH, JOINTS STAINED, SOME JOINTS MAY SHOW THIN CLAY COATINGS IF OPEN. CRYSTALS ON A BROKEN SPECIMEN FACE SHINE BRIGHTLY. ROCK RINGS UNDER HAMMER BLOWS IF OF A CRYSTALLINE NATURE.
SLIGHT (SL.)	ROCK GENERALLY FRESH, JOINTS STAINED AND DISCOLORATION EXTENDS INTO ROCK UP TO 1 INCH. OPEN JOINTS MAY CONTAIN CLAY. IN GRANITOID ROCKS SOME OCCASIONAL FELDSPAR CRYSTALS ARE DULL AND DISCOLORED. CRYSTALLINE ROCKS RING UNDER HAMMER BLOWS.
MODERATE (MOD.)	SIGNIFICANT PORTIONS OF ROCK SHOW DISCOLORATION AND WEATHERING EFFECTS. IN GRANITOID ROCKS, MOST FELDSPARS ARE DULL AND DISCOLORED, SOME SHOW CLAY. ROCK HAS DULL SOUND UNDER HAMMER BLOWS AND SHOWS SIGNIFICANT LOSS OF STRENGTH AS COMPARED WITH FRESH ROCK.
MODERATELY SEVERE (MOD. SEV.)	ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. IN GRANITOID ROCKS, ALL FELDSPARS DULL AND DISCOLORED AND A MAJORITY SHOW KAOLINIZATION. ROCK SHOWS SEVERE LOSS OF STRENGTH AND CAN BE EXCAVATED WITH A GEOLOGIST'S PICK. ROCK GIVES "CLUNK" SOUND WHEN STRUCK. <i>IF TESTED, WOULD YIELD SPT REFUSAL</i>
SEVERE (SEV.)	ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC CLEAR AND EVIDENT BUT REDUCED IN STRENGTH TO STRONG SOIL. IN GRANITOID ROCKS ALL FELDSPARS ARE KAOLINIZED TO SOME EXTENT. SOME FRAGMENTS OF STRONG ROCK USUALLY REMAIN. <i>IF TESTED, WOULD YIELD SPT N VALUES > 100 BPF</i>
VERY SEVERE (V SEV.)	ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC ELEMENTS ARE DISCERNIBLE BUT MASS IS EFFECTIVELY REDUCED TO SOIL STATUS, WITH ONLY FRAGMENTS OF STRONG ROCK REMAINING. SAPROLITE IS AN EXAMPLE OF ROCK WEATHERED TO A DEGREE THAT ONLY MINOR VESTIGES OF ORIGINAL ROCK FABRIC REMAIN. <i>IF TESTED, WOULD YIELD SPT N VALUES < 100 BPF</i>
COMPLETE	ROCK REDUCED TO SOIL. ROCK FABRIC NOT DISCERNIBLE, OR DISCERNIBLE ONLY IN SMALL AND SCATTERED CONCENTRATIONS. QUARTZ MAY BE PRESENT AS DIKES OR STRINGERS. SAPROLITE IS ALSO AN EXAMPLE.

ROCK HARDNESS

VERY HARD	CANNOT BE SCRATCHED BY KNIFE OR SHARP PICK. BREAKING OF HAND SPECIMENS REQUIRES SEVERAL HARD BLOWS OF THE GEOLOGIST'S PICK.
HARD	CAN BE SCRATCHED BY KNIFE OR PICK ONLY WITH DIFFICULTY. HARD HAMMER BLOWS REQUIRED TO DETACH HAND SPECIMEN.
MODERATELY HARD	CAN BE SCRATCHED BY KNIFE OR PICK. GOUGES OR GROOVES TO 0.25 INCHES DEEP CAN BE EXCAVATED BY HARD BLOW OF A GEOLOGIST'S PICK. HAND SPECIMENS CAN BE DETACHED BY MODERATE BLOWS.
MEDIUM HARD	CAN BE GROOVED OR GOUGED 0.05 INCHES DEEP BY FIRM PRESSURE OF KNIFE OR PICK POINT. CAN BE EXCAVATED IN SMALL CHIPS TO PIECES 1 INCH MAXIMUM SIZE BY HARD BLOWS OF THE POINT OF A GEOLOGIST'S PICK.
SOFT	CAN BE GROOVED OR GOUGED READILY BY KNIFE OR PICK. CAN BE EXCAVATED IN FRAGMENTS FROM CHIPS TO SEVERAL INCHES IN SIZE BY MODERATE BLOWS OF A PICK POINT. SMALL, THIN PIECES CAN BE BROKEN BY FINGER PRESSURE.
VERY SOFT	CAN BE CARVED WITH KNIFE. CAN BE EXCAVATED READILY WITH POINT OF PICK. PIECES 1 INCH OR MORE IN THICKNESS CAN BE BROKEN BY FINGER PRESSURE. CAN BE SCRATCHED READILY BY FINGER NAIL.

FRACTURE SPACING

TERM	SPACING
VERY WIDE	MORE THAN 10 FEET
WIDE	3 TO 10 FEET
MODERATELY CLOSE	1 TO 3 FEET
CLOSE	0.16 TO 1 FOOT
VERY CLOSE	LESS THAN 0.16 FEET

BEDDING

TERM	THICKNESS
VERY THICKLY BEDDED	4 FEET
THICKLY BEDDED	1.5 - 4 FEET
THINLY BEDDED	0.16 - 1.5 FEET
VERY THINLY BEDDED	0.03 - 0.16 FEET
THICKLY LAMINATED	0.008 - 0.03 FEET
THINLY LAMINATED	< 0.008 FEET

INDURATION

FOR SEDIMENTARY ROCKS, INDURATION IS THE HARDENING OF MATERIAL BY CEMENTING, HEAT, PRESSURE, ETC.	
FRIABLE	RUBBING WITH FINGER FREES NUMEROUS GRAINS; GENTLE BLOW BY HAMMER DISINTEGRATES SAMPLE.
MODERATELY INDURATED	GRAINS CAN BE SEPARATED FROM SAMPLE WITH STEEL PROBE; BREAKS EASILY WHEN HIT WITH HAMMER.
INDURATED	GRAINS ARE DIFFICULT TO SEPARATE WITH STEEL PROBE; DIFFICULT TO BREAK WITH HAMMER.
EXTREMELY INDURATED	SHARP HAMMER BLOWS REQUIRED TO BREAK SAMPLE; SAMPLE BREAKS ACROSS GRAINS.

TERMS AND DEFINITIONS

ALLUVIUM (ALLUV.) - SOILS THAT HAVE BEEN TRANSPORTED BY WATER.
AQUIFER - A WATER BEARING FORMATION OR STRATA.
ARENACEOUS - APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND.
ARGILLACEOUS - APPLIED TO ALL ROCKS OR SUBSTANCES COMPOSED OF CLAY MINERALS, OR HAVING A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, SUCH AS SHALE, SLATE, ETC.
ARTESIAN - GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL AT WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND SURFACE.
CALCAREOUS (CALC.) - SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE.
COLLUVIUM - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM OF SLOPE.
CORE RECOVERY (REC.) - TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED BY TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.
DIKE - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT ROCKS OR CUTS MASSIVE ROCK.
DIP - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE HORIZONTAL.
DIP DIRECTION (DIP AZIMUTH) - THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE LINE OF DIP, MEASURED CLOCKWISE FROM NORTH.
FAULT - A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE.
FISSILE - A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES.
FLOAT - ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLODGED FROM PARENT MATERIAL.
FLOOD PLAIN (FP) - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY THE STREAM.
FORMATION (FM) - A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN THE FIELD.
JOINT - FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED.
LEDGE - A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO ITS LATERAL EXTENT.
LENS - A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS.
MOTTLED (MOT.) - IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS. MOTTLING IN SOILS USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE.
PERCHED WATER - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE OF AN INTERVENING IMPERVIOUS STRATUM.
RESIDUAL (RES.) SOIL - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK.
ROCK QUALITY DESIGNATION (RQD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.
SAPROLITE (SAP.) - RESIDUAL SOIL THAT RETAINS THE RELIC STRUCTURE OR FABRIC OF THE PARENT ROCK.
SILL - AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, THAT HAS BEEN EMPLACED PARALLEL TO THE BEDDING OR SCHISTOSITY OF THE INTRUDED ROCKS.
SLICKENSIDE - POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT OR SLIP PLANE.
STANDARD PENETRATION TEST (PENETRATION RESISTANCE) (SPT) - NUMBER OF BLOWS IN OR BPF OF A 140 LB. HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1 FOOT INTO SOIL WITH A 2 INCH OUTSIDE DIAMETER SPLIT SPOON SAMPLER. SPT REFUSAL IS PENETRATION EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS.
STRATA CORE RECOVERY (SREC) - TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY TOTAL LENGTH OF STRATUM AND EXPRESSED AS A PERCENTAGE.
STRATA ROCK QUALITY DESIGNATION (SROQ) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE.
TOPSOIL (TS.) - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.

BENCH MARK: N/A

ELEVATION: N/A FEET

NOTES:

FIAD= FILLED IMMEDIATELY AFTER DRILLING



GEOTECHNICAL BORING REPORT
BORE LOG

WBS 095-01-b9ecb			TIP N/A		COUNTY WATAUGA			GEOLOGIST C. Brake								
SITE DESCRIPTION 928 James Hayes Road for Bridge over Trout Creek								GROUND WTR (ft)								
BORING NO. EB1			STATION N/A		OFFSET N/A		ALIGNMENT -L-		0 HR. 5.0							
COLLAR ELEV. 0.0 ft			TOTAL DEPTH 30.7 ft		NORTHING 901,399		EASTING 1,239,643		24 HR. FIAD							
DRILL RIG/HAMMER EFF./DATE F&R3763 CME-550X 89% 12/20/2024					DRILL METHOD H.S. Augers			HAMMER TYPE Automatic								
DRILLER W. Shenberger			START DATE 03/23/26		COMP. DATE 03/23/26		SURFACE WATER DEPTH N/A									
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	LOG	SOIL AND ROCK DESCRIPTION			
			0.5ft	0.5ft	0.5ft	0	25	50	75	100			ELEV. (ft)	DEPTH (ft)		
0													0.0	GROUND SURFACE	0.0	
	0.0	0.0	2	1	4											
-5	-3.5	3.5	31	16	14							M		-2.0	ARTIFICIAL FILL	2.0
												M7			Brown, Silty Fine to Coarse SAND (A-2-4) with Gravel	
-10	-8.5	8.5	8	15	15							W			ALLUVIAL	
															Brown-Gray, Silty Fine to Coarse Sandy GRAVEL (A-1-a) with Trace Cobble	
-15	-13.5	13.5	21	24	59							W				
-20	-18.5	18.5	100/0.3											-17.5	WEATHERED ROCK	17.5
															Tan-Gray MYLONITIC GNEISS	
	-23.5	23.5												-23.0		23.0
-25	-24.5	24.5	60/0.1											-24.5	CRYSTALLINE ROCK	24.5
			30	61	39/0.1										MYLONITIC GNEISS	
															WEATHERED ROCK	
	-28.5	28.5	7	100/0.3											Tan MYLONITIC GNEISS with intermittent Soil Layers	
-30	-30.7	30.7												-30.7		30.7
			60/0.0												Boring Terminated with Standard Penetration Test Refusal at Elevation -30.7 ft in CRYSTALLINE ROCK (MYLONITIC GNEISS)	
															Note: Driller Indicated Harder Drilling 17.5'	

NCDOT BORE SINGLE SITE 095-01-b9ECB WATAUGA COUNTY BORING LOGS.GPJ NC_DOT.GDT 4/20/26



SITE PHOTOGRAPHS:
928 James Hayes Road for Bridge over Trout Creek



Photograph No. 1: View looking North



Photograph No. 2: View looking South



Photograph No. 3: View looking upstream



Photograph No. 4: View looking downstream



SITE ID: 097-01-10fb2

SITE ADDRESS: 715 CHATHAM ST.,
RONDA, NC 28670

North Carolina Emergency Management – Private Roads and Bridges
Site Information Form

Site Number: 097-01-10fb2

Site Address: 715 Chatham Street, Ronda, NC 28670

GPS Coordinates: 36.2142,-80.9452

County: Wilkes

Bridge Type: Steel I-beam with Timber Decking or Modular Steel Bridge

Span Length: 50 ft Standard Bridge or 60 ft Modular Bridge. Refer to BSR for required waterway opening.

Bridge Width: 12'-0" Clear Width

Substructure Type: Concrete Cap on Drilled-In Piles

Geotechnical Information: See Standard Bridge Plans or the Modular Bridge Substructure Plans for Notes

Additional Notes: _____

Timber bridge railing is required for Steel I-beam with timber decking option.

Modular Steel Bridge option shall include guardrail as part of the system.

Wingwalls are not required.

The existing bridge is in place and must be removed by the Contractor prior to the start of construction.

No known debris or obstructions in the stream requiring removal.

BRIDGE SURVEY & HYDRAULIC DESIGN REPORT

NC DEPARTMENT OF EMERGENCY MANAGEMENT
PRIVATE ROADS AND BRIDGES PROGRAM

Site Number

097-01-10fb2

Latitude

36.21390

Longitude

-80.94550

County

Wilkes

Address

604 Chatham St.

City

Ronda , NC

Zip Code

28670

Recommended Structure

1 @ 60' Modular Steel Bridge (50' effective flow length)

Recommended Width of Roadway

Skew

Recommended Location is

(A) Upstream, Downstream) of Existing Crossing

Temporary Crossing



I hereby certify that that I have reviewed the existing hydraulic conveyance at this site which was a 44 ft existing bridge with the proposed conveyance provided by the proposed 60 ft. bridge.

The proposed bridge low chord for the bridge shall be set in accordance with the the FEMA Disaster Specific Guidance for the Replacement of Private Roads and Bridges issued on 14 February 2025, "to provide bridge/culvert design plans certified (sealed, signed, and dated) by a Professional Engineer licensed in the State of North Carolina demonstrating that the newly designed and installed private bridge/culvert provides conveyance greater than or equal to the original destroyed crossing".

This certification demonstrates that the newly designed and installed private bridge/culvert provides conveyance greater than or equal to the original destroyed crossing. This is based on the best available data provided from post storm evaluations. Portions of the existing structures may have been destroyed, removed, modified or shifted from their original location or elevation.

Designed by

Assisted by

Date

Signed by

Matthew D Foster

7/27/2026

12:18:31 PM EDT

Seal

20646

Professional Engineer

Matthew D. Foster

Reviewed by

Date

Initial

MDF

SITE DATA

Drainage Area

Source

River Basin

Yadkin River

Character

Stream Classification (e.g., Trout, High Quality Water)

WS-IV, (for the Yadkin River. UT has no Class).

Debris Potential: Low

☐ Moderate

☒ High

☐

Existing Structure - Source of Available Data

NCEM Private Roads and Bridges Inspection Team

Existing Structure - Description

1 @ 44'+/- private bridge (damaged by Helene)

Estimated Waterway Opening

341.0

ft²

Design Control Elev

ft

Source

Gage Station No

Period of Records

Max Discharge

cfs

Date

Frequency

Historical Flood Information:

Date

Elev

ft

Est Freq

yr

Source

Period of Knowledge

yrs

Historical Scour Info: General

ft

Contraction

ft

Local

ft

Channel Slope

ft/ft

Source

Normal Water Surface Elev

ft

Manning's n: Left OB

Channel

Right OB

Source

Flood Study / Status

N/A (UT to Yadkin River). Note - bridge is subject to backwater from Yadkin River

Flood Study

100-yr Discharge

cfs

WS Elev: Floodway

ft

Without Floodway

ft

River Station

DESIGN DATA

Hydrological Method

Disaster Specific Guidance for the Replacement of Private Roads and Bridges 2/14/2025

Hydraulic Design Method

Floods Evaluated

Frequency (year)

Discharge (cfs)

Elevation (ft)

Backwater (ft)

Bridge Opening Velocity (fps)

Waterway Opening Provided Below: Design WS Elev

sf

100-yr WS Elev

sf

Total

409.8

sf

Average Channel Velocity (Design)

fps

Average Overbank Velocity (Design)

fps

Computed Scour: General

ft

Contraction

ft

Local

ft

INFORMATION TO BE SHOWN ON PLANS

HYDRAULIC DATA

DESIGN DISCHARGE

= 280

C.F.S.

FREQUENCY OF DESIGN FLOOD

= 25

YRS.

DESIGN HIGH WATER ELEVATION

=

DRAINAGE AREA

= 0.44

SQ. MI.

BASIC DISCHARGE (Q100)

= 390

C.F.S.

BASIC HIGH WATER ELEVATION

=

OVERTOPPING FLOOD DATA

OVERTOPPING DISCHARGE

=

C.F.S.

FREQUENCY OF OVERTTOPPING FLOOD

=

YRS.

OVERTOPPING FLOOD ELEVATION

=

"

*NOTE LOCATION OF OVERTOPPING

WS EL. Taken @ River Station ?

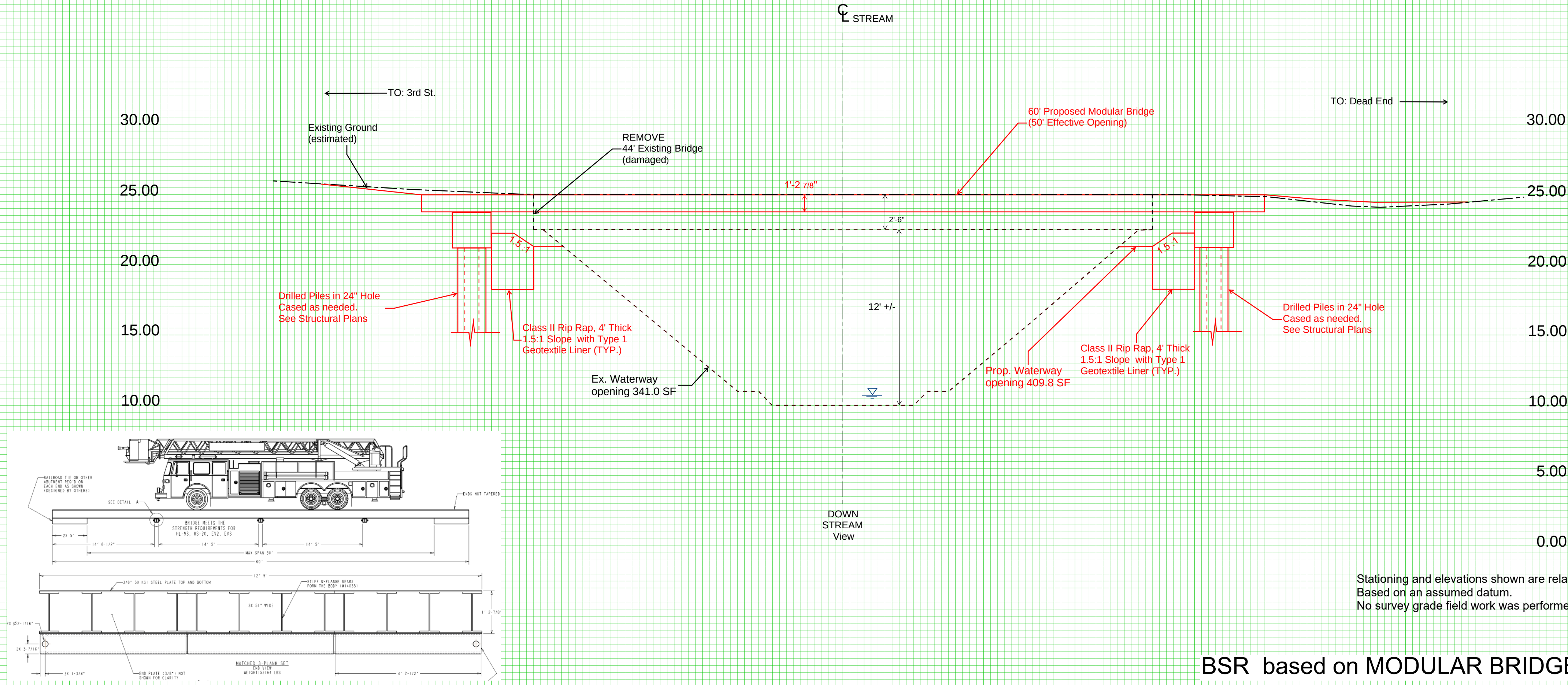
ADDITIONAL INFORMATION AND COMPUTATIONS

Emergency Vehicle Access Possible?	No
Number of Homes Confirmed	Yes
Number of Homes	4
Churches Confirmed	Yes
Number of Churches	0
Schools Confirmed	Yes
Number of Schools	0
Recreational/Business Areas Confirmed	Yes
Number of Recreational/Business Areas	1
General Description	Bridge is constructed of concrete end bents, steel beams, and wooden deck and rails. It is a one span bridge. It is damaged beyond repair and a redesign and replacement is needed.
Overall Condition	Damage
Condition Other	
Site Repair Status	No Repair
Condition Description	Bridge is damaged beyond repair. Apparently, rising water pushed up the leading edge of the bridge and it appears one beam is missing and others may have moved off their seats.
Expected Level of Effort	Full Redesign
Other Level of Effort	
Horizontal Curve	No
Number of Travel Lanes (LOS)	1
Inclination	No
Roadway Divider	No
Road/Bridge Width (ft)	17.00
Span/Gap Estimate (ft)	46.00
Surface to Water (ft)	15.00
Utility/Mechanical	No

14" W14X38 beam
+ 0.25" Steel Plate
+ 0.25" Steel Plate
=14.5" (1'-2.5") ft structure depth)

Proposed Conveyance Area has been reduced by 0.9 sf to account for blockage created by 3 Plank Connectors as shown in Detail A of the Typical Section.

10+00 10+05 10+10 10+15 10+20 10+25 10+30 10+35 10+40 10+45 10+50 10+55 10+60 10+65 10+70



Stationing and elevations shown are relative to the site. Based on an assumed datum. No survey grade field work was performed.

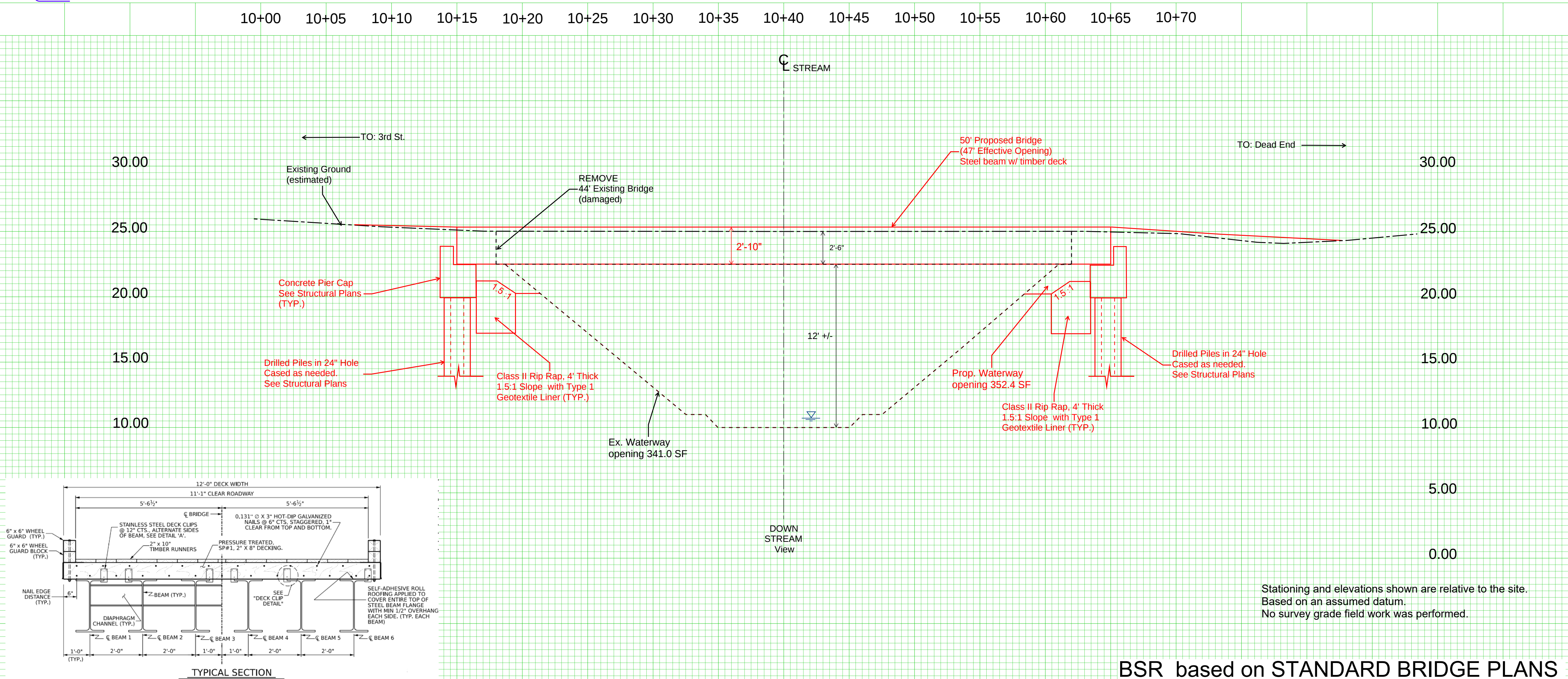
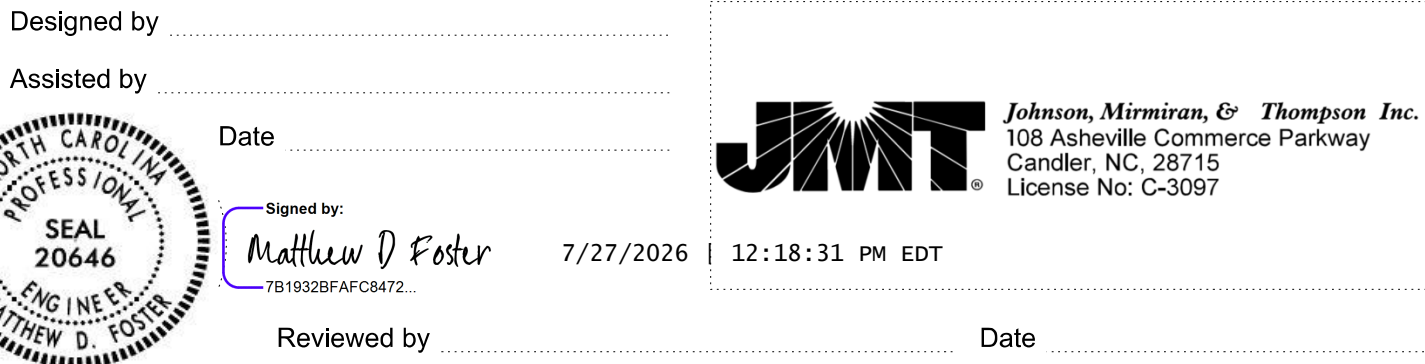
BSR based on MODULAR BRIDGE PLANS

NC DEPARTMENT OF EMERGENCY MANAGEMENT
PRIVATE ROADS AND BRIDGES PROGRAM

Recommended Width of Roadway Skew

Recommended Location is (At) Upstream, Downstream) of Existing Crossing

Temporary Crossing



GEOTECHNICAL BORING REPORT
BORE LOG

WBS 097-01-10fb2			TIP N/A		COUNTY WILKES		GEOLOGIST C. Brake								
SITE DESCRIPTION 715 Chatham Street Bridge over Dam Tailwater to Yadkin River							GROUND WTR (ft)								
BORING NO. EB1		STATION N/A		OFFSET N/A		ALIGNMENT -L-		0 HR.	18.4						
COLLAR ELEV. 0.0 ft		TOTAL DEPTH 38.7 ft		NORTHING 902,509		EASTING 1,426,164		24 HR.	15.5						
DRILL RIG/HAMMER EFF./DATE F&R3763 CME-550X 89% 12/20/2024				DRILL METHOD H.S. Augers			HAMMER TYPE Automatic								
DRILLER S. Davis		START DATE 03/11/26		COMP. DATE 03/11/26		SURFACE WATER DEPTH N/A									
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	LOG	SOIL AND ROCK DESCRIPTION		
			0.5ft	0.5ft	0.5ft	0	25	50	75	100			ELEV. (ft)	DEPTH (ft)	
0													0.0	GROUND SURFACE	0.0
-5	0.0	0.0	5	4	3							M	ARTIFICIAL FILL	Gray, Silty Fine to Coarse SAND (A-2-4) with Some Gravel	-2.0
	-3.5	3.5	2	2	1							M			
-10													ALLUVIAL	Brown, Fine Sandy SILT (A-4) with Trace Mica	-7.0
	-8.5	8.5	WOH	1	1							M			
-15													RESIDUAL	Brown, Fine to Coarse Sandy SILT (A-4) with Trace Mica and Rock Fragments	-12.0
	-13.5	13.5	WOH	WOH	1							M			
-20													WEATHERED ROCK	Brown, Gray, and Tan MYLONITIC MICA SCHIST	-17.5
	-18.5	18.5	36	36	30							M			
-25													Note: Driller noted harder drilling at 17.5 feet.		
	-23.5	23.5	29	64	36/0.1										
-30															
	-28.5	28.5	100/0.2												
-35															
	-33.5	33.5	74	26/0.1											
	-38.5	38.5	100/0.2												

NCDOT BORE SINGLE SITE 097-01-10FB2 WILKES COUNTY BORING LOGS.GPJ NC_DOT.GDT 3/25/26

GEOTECHNICAL BORING REPORT
BORE LOG

WBS 097-01-10fb2		TIP N/A		COUNTY WILKES		GEOLOGIST C. Brake											
SITE DESCRIPTION 715 Chatham Street Bridge over Dam Tailwater to Yadkin River							GROUND WTR (ft)										
BORING NO. EB2		STATION N/A		OFFSET N/A		ALIGNMENT -L-		0 HR. Dry									
COLLAR ELEV. 0.0 ft		TOTAL DEPTH 29.8 ft		NORTHING 902,462		EASTING 1,426,135		24 HR. 20.0									
DRILL RIG/HAMMER EFF./DATE F&R3763 CME-550X 89% 12/20/2024				DRILL METHOD H.S. Augers			HAMMER TYPE Automatic										
DRILLER S. Davis		START DATE 03/11/26		COMP. DATE 03/11/26		SURFACE WATER DEPTH N/A											
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	MOI	LOG	SOIL AND ROCK DESCRIPTION			
			0.5ft	0.5ft	0.5ft	0	25	50	75	100				ELEV. (ft)	DEPTH (ft)		
0														0.0	GROUND SURFACE	0.0	
	0.0	0.0	6	7	5							M		-1.0	ARTIFICIAL FILL	1.0	
	-3.5	3.5	4	5	10							M		-2.0	Gray, Silty Fine to Coarse SAND (A-2-4) with Some Gravel	2.0	
-5															Red-Brown, Fine to Coarse Sandy Silty CLAY (A-7) with Trace Gravel and Roots		
	-8.5	8.5	12	12	16							M		-7.0	RESIDUAL	7.0	
-10															Orange-Tan, Fine to Coarse Sandy Clayey SILT (A-5) with Trace Mica and Rock Fragments		
	-13.5	13.5	28	50	50/0.4										Brown-Tan, Fine to Coarse Sandy SILT (A-4) with Trace Mica and Rock Fragments		
-15														-14.0	WEATHERED ROCK	14.0	
	-18.5	18.5	100/0.4												Tan-Gray MYLONITIC MICA SCHIST		
-20																	
	-23.5	23.5	100/0.4														
-25																	
	-28.5	28.5	38	42	58/0.3												
														-29.8	Boring Terminated at Elevation -29.8 ft in WEATHERED ROCK (MYLONITIC MICA SCHIST)	29.8	

DRAFT



BOBBY & HOPE SHEETS

SUZAN MYERS

BRIDGE LOCATION

JERRY SIDEN

HORACIO LOPEZ

SITE ID: 097-01-132d4

SITE ADDRESS: 1089 ANNIE-SOPHIA LANE
ROARING RIVER, NC 28669

North Carolina Emergency Management – Private Roads and Bridges
Site Information Form

Site Number: 097-01-132d4

Site Address: 1089 Annie Sophia Lane, Roaring River, NC 28669

GPS Coordinates: 36.2813,-80.9680

County: Wilkes

Bridge Type: Steel I-beam with Timber Decking or Modular Steel Bridge

Span Length: 30 ft Standard Bridge or 40 ft Modular Bridge. Refer to BSR for required waterway opening.

Bridge Width: 12'-0" Clear Width

Substructure Type: Concrete Cap on Drilled-in Piles

Geotechnical Information: See Standard Bridge Plans or the Modular Bridge Substructure Plans for Notes

Additional Notes: _____

Timber bridge railing not required for Steel I-beam with timber decking option.

Modular Steel Bridge option shall include guardrail as part of the system.

Wingwalls are not required.

The existing bridge is in place and must be removed by the Contractor prior to the start of construction.

No known debris or obstructions in the stream requiring removal.

BRIDGE SURVEY & HYDRAULIC DESIGN REPORT

NC DEPARTMENT OF EMERGENCY MANAGEMENT
PRIVATE ROADS AND BRIDGES PROGRAM

Site Number097-01-132d4Latitude36.28129Longitude-80.968050

CountyWilkesAddressnear 1089 Annie Sophia Lane

CityRoaring River, NCZip Code28669

Recommended Structure1 @ 30" Steel Girder Bridge with timber deck

Recommended Width of RoadwaySkew

Recommended Location is (At)Upstream, Downstream) of Existing Crossing

Temporary Crossing



I hereby certify that that I have reviewed the existing hydraulic conveyance at this site which was a 2@48" CMP existing culverts with the proposed conveyance provided by the proposed 30 ft. bridge.

The proposed bridge low chord for the bridge shall be set in accordance with the the FEMA Disaster Specific Guidance for the Replacement of Private Roads and Bridges issued on 14 February 2025, "to provide bridge/culvert design plans certified (sealed, signed, and dated) by a Professional Engineer licensed in the State of North Carolina demonstrating that the newly designed and installed private bridge/culvert provides conveyance greater than or equal to the original destroyed crossing".

This certification demonstrates that the newly designed and installed private bridge/culvert provides conveyance greater than or equal to the original destroyed crossing. This is based on the best available data provided from post storm evaluations. Portions of the existing structures may have been destroyed, removed, modified or shifted from their original location or elevation.

Designed by

Assisted by

Date

Signed by:Matthew D Foster6/10/202610:54:34 AM EDT

Reviewed by

Date

Professional Engineer Seal: Matthew D. Foster, No. 20646

Johnson, Mirmiran, & Thompson Inc. 108 Asheville Commerce Parkway Candler, NC, 28715 License No: C-3097

SITE DATA

Drainage AreaSource

River BasinYadkin Pee-DeeCharacter

Stream Classification (e.g., Trout, High Quality Water)Class C

Debris Potential: LowModerateHigh

Existing Structure - Source of Available DataNCEM Private Roads and Bridges Inspection Team

Existing Structure - Description2 @ 48 inch CMP

Estimated Waterway Opening25.1ft²

Design Control ElevftSource

Gage Station NoPeriod of Records

Max DischargecfsDateFrequency

Historical Flood Information:

DateElevftEst FreqyrSourcePeriod of Knowledgeyrs

Historical Scour Info: GeneralftContractionftLocalft

Channel Slopeft/ftSourceNormal Water Surface Elevft

Manning's n: Left OBChannelRight OBSource

Flood Study / StatusFEMA Study LDS (Big Bugaboo Creek)

Flood Study1732cfsWS Elev: 1187.15ftWithout Floodway1186.46ftRiver Station32578

DESIGN DATA

Hydrological Method

Hydraulic Design MethodDisaster Specific Guidance for the Replacement of Private Roads and Bridges 2/14/2025

Floods EvaluatedFrequency (year)Discharge (cfs)Elevation (ft)Backwater (ft)Bridge Opening Velocity (fps)

Waterway Opening Provided Below: Design WS Elevsf100-yr WS ElevsfTotal83.6sf

Average Channel Velocity (Design)fpsAverage Overbank Velocity (Design)fps

Computed Scour: GeneralftContractionftLocalft

INFORMATION TO BE SHOWN ON PLANS

HYDRAULIC DATA

DESIGN DISCHARGE= 1130_ C.F.S.

FREQUENCY OF DESIGN FLOOD= 25_ YRS.

DESIGN HIGH WATER ELEVATION=

DRAINAGE AREA= 3.88_ SQ. MI.

BASIC DISCHARGE (Q100)= 1640_ C.F.S.

BASIC HIGH WATER ELEVATION=

OVERTOPPING FLOOD DATA

OVERTOPPING DISCHARGE= C.F.S.

FREQUENCY OF OVERTTOPPING FLOOD= YRS.

OVERTOPPING FLOOD ELEVATION= *

*NOTE LOCATION OF OVERTOPPING

WS EL. Taken @ River Station ?

ADDITIONAL INFORMATION AND COMPUTATIONS

Number of Homes ConfirmedYes

Number of Homes10

Churches ConfirmedYes

Number of Churches0

Schools ConfirmedYes

Number of Schools0

Recreational/Business Areas ConfirmedYes

Number of Recreational/Business Areas0

General DescriptionRoad and culvert crossing are severely damaged. Crossing consists of 2-48" CMP.

Overall ConditionDamage

Condition Other

Site Repair StatusTemporary Repair

Condition DescriptionRoad and culvert crossing are in poor condition and appear to be undersized. Replacement culverts need to be sized properly with endwalls. Estimate includes replacement of the culvert at the same size and will need to be revised once sized properly.

Expected Level of EffortReplace

Other Level of Effort

Horizontal CurveNo

Number of Travel Lanes (LOS)1

InclinationNo

Roadway DividerNo

Road/Bridge Width (ft)11.00

Spew/Gap Estimate (ft)

Surface to Water (ft)5.00

Utility/MechanicalNo

Utility Types

Pipe Needs SizingYes

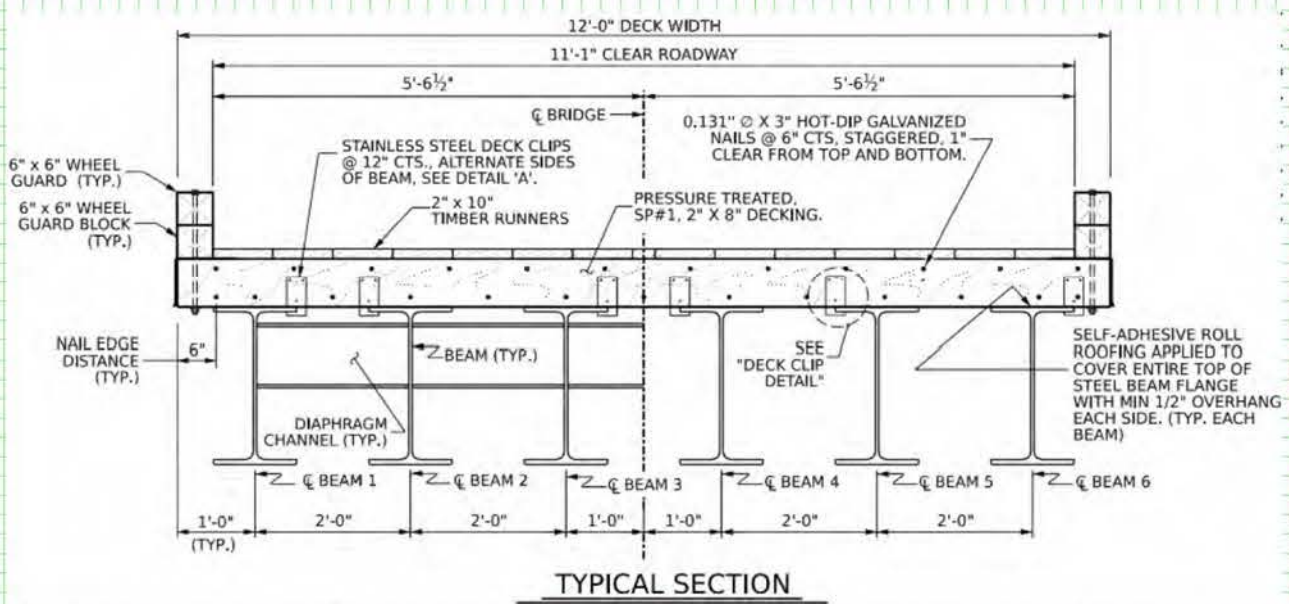
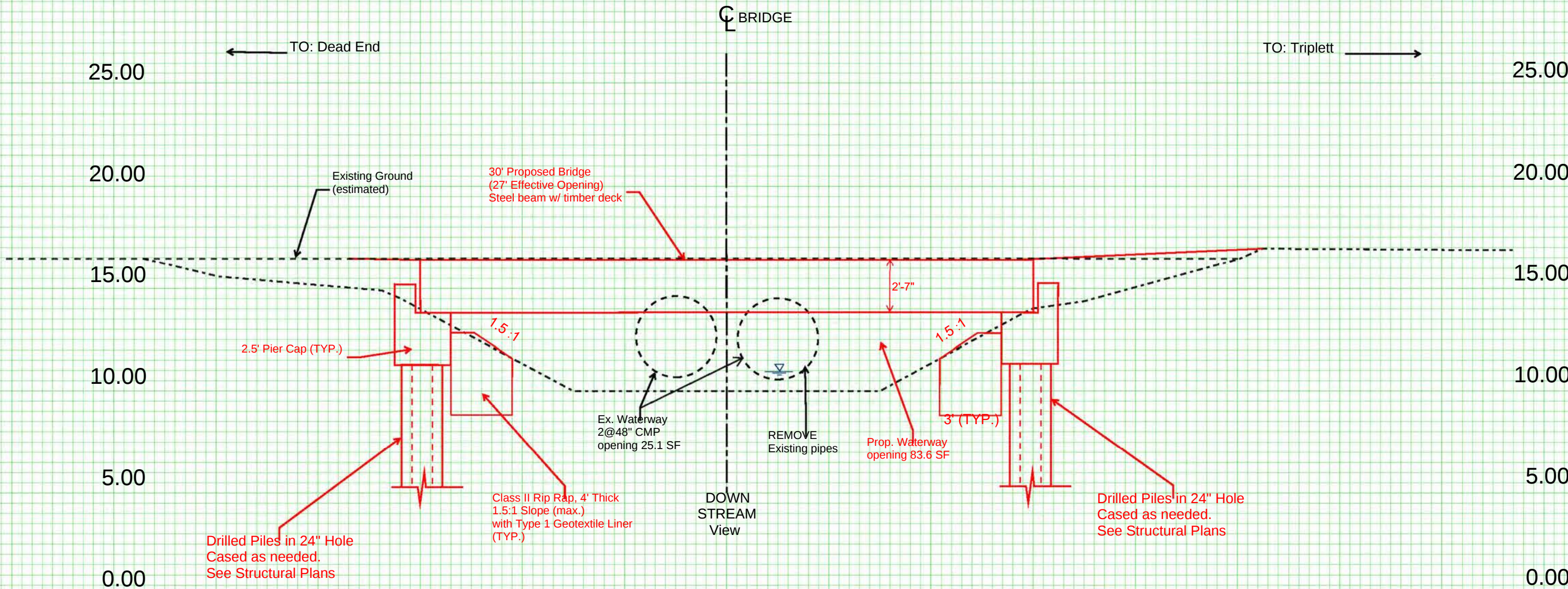
Depth of Pipe1.00

GeotechnicalOther

Other GeotechnicalNone

Proposed 21" W21X48 beam + 8" Deck + 2" Runner =31" (2'-7" structure depth)

10+00 10+05 10+10 10+15 10+20 10+25 10+30 10+35 10+40 10+45 10+50 10+55 10+60 10+65 10+70



Stationing and elevations shown are relative to the site. Based on an assumed datum. No survey grade field work was performed.

BSR based on STANDARD BRIDGE PLANS

BRIDGE SURVEY & HYDRAULIC DESIGN REPORT

NC DEPARTMENT OF EMERGENCY MANAGEMENT
PRIVATE ROADS AND BRIDGES PROGRAM

Site Number097-01-132d4Latitude36.28129Longitude-80.968050

CountyWilkesAddressnear 1089 Annie Sophia Lane

CityRoaring River, NCZip Code28669

Recommended Structure1 @ 40' Steel Modular Bridge (30' effective length)

Recommended Width of RoadwaySkew

Recommended Location is (At)Upstream, Downstream) of Existing Crossing

Temporary Crossing



I hereby certify that I have reviewed the existing hydraulic conveyance at this site which was a 2@48" CMP existing culverts with the proposed conveyance provided by the proposed 40 ft. bridge.

The proposed bridge low chord for the bridge shall be set in accordance with the FEMA Disaster Specific Guidance for the Replacement of Private Roads and Bridges issued on 14 February 2025, "to provide bridge/culvert design plans certified (sealed, signed, and dated) by a Professional Engineer licensed in the State of North Carolina demonstrating that the newly designed and installed private bridge/culvert provides conveyance greater than or equal to the original destroyed crossing".

This certification demonstrates that the newly designed and installed private bridge/culvert provides conveyance greater than or equal to the original destroyed crossing. This is based on the best available data provided from post storm evaluations. Portions of the existing structures may have been destroyed, removed, modified or shifted from their original location or elevation.

Designed by

Assisted by

North Carolina Professional Engineer Seal 20646 Matthew D. Foster

Signature of Matthew D. Foster

Date

6/10/2026

Reviewed by

Johnson, Mirmiran, & Thompson Inc.

108 Asheville Commerce Parkway

Candler, NC, 28715

License No: C-3097

10:54:34 AM EDT

Date

SITE DATA

Drainage AreaSource

River BasinYadkin Pee-DeeCharacter

Stream Classification (e.g., Trout, High Quality Water)Class C

Debris Potential: Low Moderate High

Existing Structure - Source of Available DataNCEM Private Roads and Bridges Inspection Team

Existing Structure - Description2 @ 48 inch CMP

Estimated Waterway Opening25.1ft²

Design Control Elevft Source

Gage Station NoPeriod of Records

Max DischargecfsDateFrequency

Historical Flood Information:

DateElevftEst FreqyrSourcePeriod of Knowledgeyrs

Historical Scour Info: GeneralftContractionftLocalft

Channel Slopeft/ft SourceNormal Water Surface Elevft

Manning's n: Left OBChannelRight OBSource

Flood Study / StatusFEMA Study LDS (Big Bugaboo Creek)

Flood Study1732cfs WS Elev: 1187.15ft Without Floodway1186.46ft River Station32578

DESIGN DATA

Hydrological Method

Hydraulic Design MethodDisaster Specific Guidance for the Replacement of Private Roads and Bridges 2/14/2025

Floods Evaluated	Frequency (year)	Discharge (cfs)	Elevation (ft)	Backwater (ft)	Bridge Opening Velocity (fps)

Waterway Opening Provided Below: Design WS Elevsf100-yr WS ElevsfTotal130.3sf

Average Channel Velocity (Design)fpsAverage Overbank Velocity (Design)fps

Computed Scour: GeneralftContractionftLocalft

INFORMATION TO BE SHOWN ON PLANS

HYDRAULIC DATA

DESIGN DISCHARGE= 1130_ C.F.S.

FREQUENCY OF DESIGN FLOOD= 25_ YRS.

DESIGN HIGH WATER ELEVATION=

DRAINAGE AREA= 3.88_ SQ. MI.

BASIC DISCHARGE (Q100)= 1640_ C.F.S.

BASIC HIGH WATER ELEVATION=

OVERTOPPING FLOOD DATA

OVERTOPPING DISCHARGE= C.F.S.

FREQUENCY OF OVERTTOPPING FLOOD= YRS.

OVERTOPPING FLOOD ELEVATION= *

*NOTE LOCATION OF OVERTOPPING

WS EL. Taken @ River Station ?

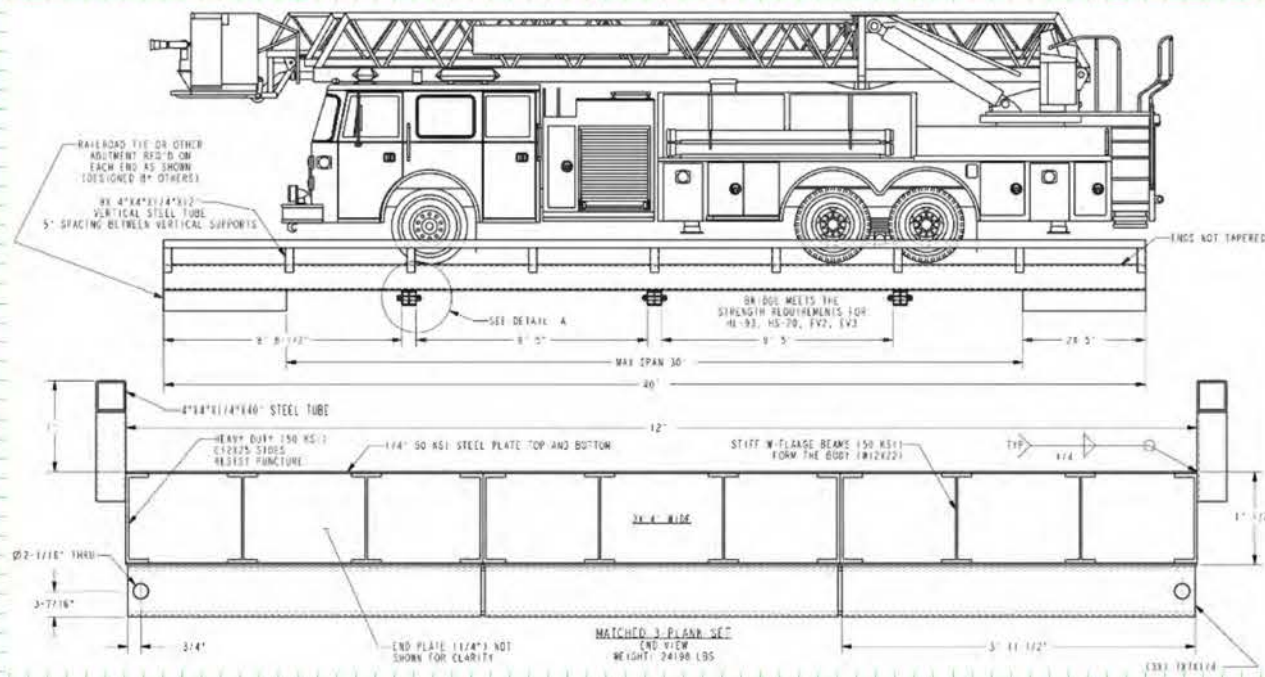
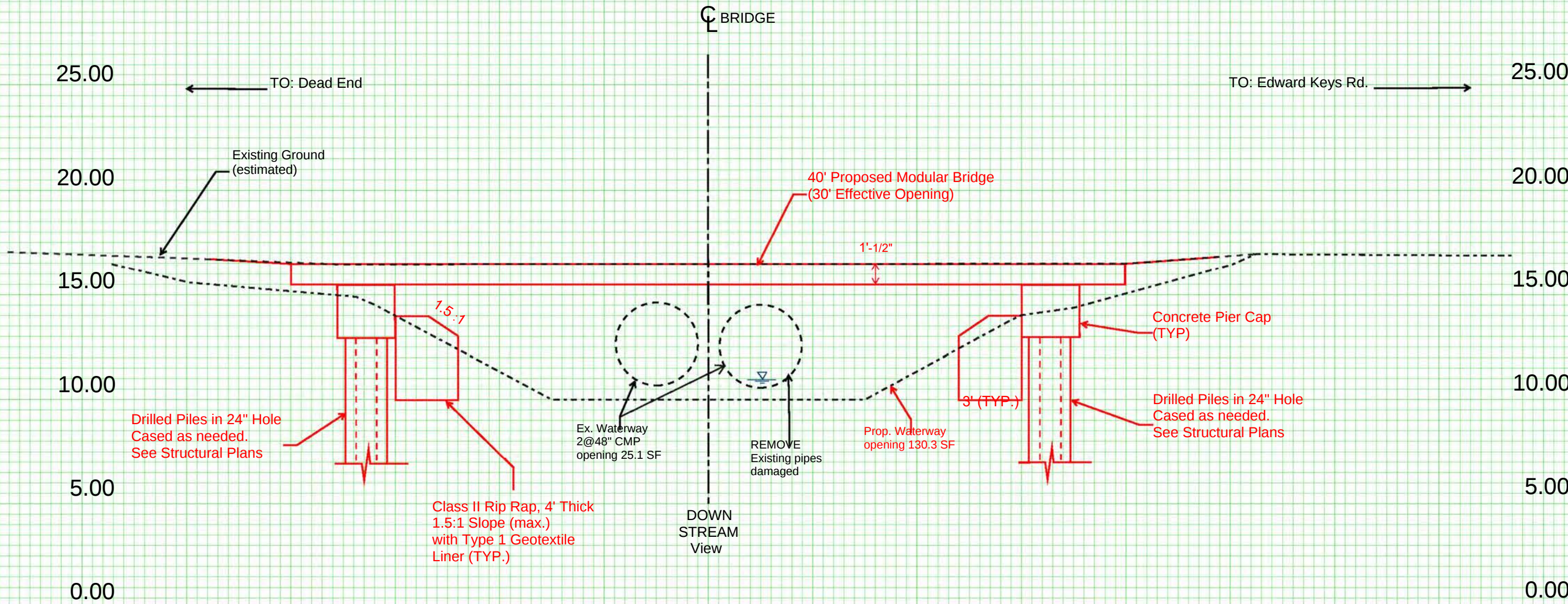
ADDITIONAL INFORMATION AND COMPUTATIONS

Number of Homes Confirmed	Yes
Number of Homes	10
Churches Confirmed	Yes
Number of Churches	0
Schools Confirmed	Yes
Number of Schools	0
Recreational/Business Areas Confirmed	Yes
Number of Recreational/Business Areas	0
General Description	Road and culvert crossing are severely damaged. Crossing consists of 2-48" CMP.
Overall Condition	Damage
Condition Other	
Site Repair Status	Temporary Repair
Condition Description	Road and culvert crossing are in poor condition and appear to be undersized. Replacement culverts need to be sized properly with endwalls. Estimate includes replacement of the culvert at the same size and will need to be revised once sized properly.
Expected Level of Effort	Replace
Other Level of Effort	
Horizontal Curve	No
Number of Travel Lanes (LOS)	1
Inclination	No
Roadway Divider	No
Road/Bridge Width (ft)	11.00
Spew/Gap Estimate (ft)	
Surface to Water (ft)	5.00
Utility/Mechanical	No
Utility Types	
Pipe Needs Sizing	Yes
Depth of Pipe	1.00
Geotechnical	Other
Other Geotechnical	None

12" W121X25 beam
+ 0.25" Steel Plate
+ 0.25" Steel Plate
=12.5" (1'-1/2") ft structure depth

Proposed Conveyance Area has been reduced by 0.9 sf to account for blockage created by 3 Plank Connectors as shown in Detail A of the Typical Section.

10+00 10+05 10+10 10+15 10+20 10+25 10+30 10+35 10+40 10+45 10+50 10+55 10+60 10+65 10+70



Stationing and elevations shown are relative to the site.
Based on an assumed datum.
No survey grade field work was performed.

BSR based on MODULAR BRIDGE PLANS

REFERENCE: N/A

PROJECT: N/A

STATE	STATE PROJECT REFERENCE NO.	SHEET NO.	TOTAL SHEETS
N.C.	097-01-132d4	1	

STATE OF NORTH CAROLINA
DEPARTMENT OF TRANSPORTATION
DIVISION OF HIGHWAYS
GEOTECHNICAL ENGINEERING UNIT

STRUCTURE
SUBSURFACE INVESTIGATION

COUNTY WILKES

PROJECT DESCRIPTION NORTH CAROLINA EMERGENCY
MANAGEMENT-PRIVATE ROADS, BRIDGE REPAIR
AND REPLACEMENT PROGRAM

SITE DESCRIPTION 1089 ANNE-SOPHIA LANE FOR
BRIDGE OVER BIG BUGABOO CREEK

CONTENTS

<u>SHEET NO.</u>	<u>DESCRIPTION</u>
1	TITLE SHEET
2, 2A	LEGEND (SOIL & ROCK)
2B, 2C	SUPPLEMENTAL LEGEND (GSI)
3	SITE PLAN
4-7	BORE LOG(S), CORE REPORT(S), & CORE PHOTOGRAPH(S)
8-9	SITE PHOTOGRAPH(S)

PERSONNEL

C. BRAKE, G.I.T.

S. DAVIS

TY. BEARD

INVESTIGATED BY F&R, Inc.

DRAWN BY T.T. WALKER

CHECKED BY P. ALTON, P.E.

SUBMITTED BY P. ALTON, P.E.

DATE APRIL 2026

CAUTION NOTICE

THE SUBSURFACE INFORMATION AND THE SUBSURFACE INVESTIGATION ON WHICH IT IS BASED WERE MADE FOR THE PURPOSE OF STUDY, PLANNING AND DESIGN, AND NOT FOR CONSTRUCTION OR PAY PURPOSES.

GENERAL SOIL AND ROCK STRATA DESCRIPTIONS AND INDICATED BOUNDARIES ARE BASED ON A GEOTECHNICAL INTERPRETATION OF ALL AVAILABLE SUBSURFACE DATA AND MAY NOT NECESSARILY REFLECT THE ACTUAL SUBSURFACE CONDITIONS BETWEEN BORINGS OR BETWEEN SAMPLED STRATA WITHIN THE BOREHOLE. THE LABORATORY SAMPLE DATA AND THE IN SITU (IN-PLACE) TEST DATA CAN BE RELIED ON ONLY TO THE DEGREE OF RELIABILITY INHERENT IN THE STANDARD TEST METHOD. THE OBSERVED WATER LEVELS OR SOIL MOISTURE CONDITIONS INDICATED IN THE SUBSURFACE INVESTIGATIONS ARE AS RECORDED AT THE TIME OF THE INVESTIGATION. THESE WATER LEVELS OR SOIL MOISTURE CONDITIONS MAY VARY CONSIDERABLY WITH TIME ACCORDING TO CLIMATIC CONDITIONS INCLUDING TEMPERATURES, PRECIPITATION AND WIND, AS WELL AS OTHER NON-CLIMATIC FACTORS.

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NOTES:

1. THE INFORMATION CONTAINED HEREIN IS NOT IMPLIED OR GUARANTEED BY THE GEOTECHNICAL ENGINEER AS ACCURATE NOR IS IT CONSIDERED PART OF THE PLANS, SPECIFICATIONS OR CONTRACT FOR THE PROJECT.
2. BY HAVING REQUESTED THIS INFORMATION, THE CONTRACTOR SPECIFICALLY WAIVES ANY CLAIMS FOR INCREASED COMPENSATION OR EXTENSION OF TIME BASED ON DIFFERENCES BETWEEN THE CONDITIONS INDICATED HEREIN AND THE ACTUAL CONDITIONS AT THE PROJECT SITE.

SINCE



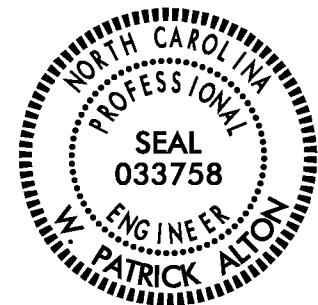
1881

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SIGNATURE

DATE

**DOCUMENT NOT CONSIDERED FINAL
UNLESS ALL SIGNATURES COMPLETED**

EQUIPMENT USED ON SUBJECT PROJECT:		
DRILL UNITS: ☐ CME-45C ☐ CME-55 ☐ CME-550 ☐ VANE SHEAR TEST ☐ PORTABLE HOIST ☒ <u>CME-750X</u> ☐	ADVANCING TOOLS: ☐ CLAY BITS ☐ 6" CONTINUOUS FLIGHT AUGER ☒ 8" HOLLOW AUGERS ☐ HARD FACED FINGER BITS ☐ TUNG.-CARBIDE INSERTS ☒ CASING ☒ W/ ADVANCER ☐ TRICONE _____ * STEEL TEETH ☐ TRICONE _____ * TUNG.-CARB. ☒ CORE BIT	HAMMER TYPE: ☒ AUTOMATIC ☐ MANUAL CORE SIZE: ☐ -B _____ ☐ -H _____ ☒ -N <u>Q3</u> HAND TOOLS: ☐ POST HOLE DIGGER ☐ HAND AUGER ☐ SOUNDING ROD ☐ VANE SHEAR TEST ☐

**NORTH CAROLINA DEPARTMENT OF TRANSPORTATION
DIVISION OF HIGHWAYS
GEOTECHNICAL ENGINEERING UNIT**

SUBSURFACE INVESTIGATION

SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS (PAGE 2 OF 2)

ROCK DESCRIPTION

HARD ROCK IS NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT REFUSAL IF TESTED. AN INFERRED ROCK LINE INDICATES THE LEVEL AT WHICH NON-COASTAL PLAIN MATERIAL WOULD YIELD SPT REFUSAL. SPT REFUSAL IS PENETRATION BY A SPLIT SPOON SAMPLER EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS IN NON-COASTAL PLAIN MATERIAL. THE TRANSITION BETWEEN SOIL AND ROCK IS OFTEN REPRESENTED BY A ZONE OF WEATHERED ROCK. ROCK MATERIALS ARE TYPICALLY DIVIDED AS FOLLOWS:

WEATHERED ROCK (WR)		NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT N VALUES > 100 BLOWS PER FOOT IF TESTED.
CRYSTALLINE ROCK (CR)		FINE TO COARSE GRAIN IGNEOUS AND METAMORPHIC ROCK THAT WOULD YIELD SPT REFUSAL IF TESTED. ROCK TYPE INCLUDES GRANITE, GNEISS, GABBRO, SCHIST, ETC.
NON-CRYSTALLINE ROCK (NCR)		FINE TO COARSE GRAIN METAMORPHIC AND NON-COASTAL PLAIN SEDIMENTARY ROCK THAT WOULD YIELD SPT REFUSAL IF TESTED. ROCK TYPE INCLUDES PHYLLITE, SLATE, SANDSTONE, ETC.
COASTAL PLAIN SEDIMENTARY ROCK (CPS)		COASTAL PLAIN SEDIMENTS CEMENTED INTO ROCK, BUT MAY NOT YIELD SPT REFUSAL. ROCK TYPE INCLUDES LIMESTONE, SANDSTONE, CEMENTED SHELL BEDS, ETC.

WEATHERING

FRESH	ROCK FRESH, CRYSTALS BRIGHT, FEW JOINTS MAY SHOW SLIGHT STAINING. ROCK RINGS UNDER HAMMER IF CRYSTALLINE.
VERY SLIGHT (V SL.)	ROCK GENERALLY FRESH, JOINTS STAINED, SOME JOINTS MAY SHOW THIN CLAY COATINGS IF OPEN. CRYSTALS ON A BROKEN SPECIMEN FACE SHINE BRIGHTLY. ROCK RINGS UNDER HAMMER BLOWS IF OF A CRYSTALLINE NATURE.
SLIGHT (SL.)	ROCK GENERALLY FRESH, JOINTS STAINED AND DISCOLORATION EXTENDS INTO ROCK UP TO 1 INCH. OPEN JOINTS MAY CONTAIN CLAY. IN GRANITOID ROCKS SOME OCCASIONAL FELDSPAR CRYSTALS ARE DULL AND DISCOLORED. CRYSTALLINE ROCKS RING UNDER HAMMER BLOWS.
MODERATE (MOD.)	SIGNIFICANT PORTIONS OF ROCK SHOW DISCOLORATION AND WEATHERING EFFECTS. IN GRANITOID ROCKS, MOST FELDSPARS ARE DULL AND DISCOLORED, SOME SHOW CLAY. ROCK HAS DULL SOUND UNDER HAMMER BLOWS AND SHOWS SIGNIFICANT LOSS OF STRENGTH AS COMPARED WITH FRESH ROCK.
MODERATELY SEVERE (MOD. SEV.)	ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. IN GRANITOID ROCKS, ALL FELDSPARS DULL AND DISCOLORED AND A MAJORITY SHOW KAOLINIZATION. ROCK SHOWS SEVERE LOSS OF STRENGTH AND CAN BE EXCAVATED WITH A GEOLOGIST'S PICK. ROCK GIVES "CLUNK" SOUND WHEN STRUCK. <i>IF TESTED, WOULD YIELD SPT REFUSAL</i>
SEVERE (SEV.)	ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC CLEAR AND EVIDENT BUT REDUCED IN STRENGTH TO STRONG SOIL. IN GRANITOID ROCKS ALL FELDSPARS ARE KAOLINIZED TO SOME EXTENT. SOME FRAGMENTS OF STRONG ROCK USUALLY REMAIN. <i>IF TESTED, WOULD YIELD SPT N VALUES > 100 BPF</i>
VERY SEVERE (V SEV.)	ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC ELEMENTS ARE DISCERNIBLE BUT MASS IS EFFECTIVELY REDUCED TO SOIL STATUS, WITH ONLY FRAGMENTS OF STRONG ROCK REMAINING. SAPROLITE IS AN EXAMPLE OF ROCK WEATHERED TO A DEGREE THAT ONLY MINOR VESTIGES OF ORIGINAL ROCK FABRIC REMAIN. <i>IF TESTED, WOULD YIELD SPT N VALUES < 100 BPF</i>
COMPLETE	ROCK REDUCED TO SOIL. ROCK FABRIC NOT DISCERNIBLE, OR DISCERNIBLE ONLY IN SMALL AND SCATTERED CONCENTRATIONS. QUARTZ MAY BE PRESENT AS DIKES OR STRINGERS. SAPROLITE IS ALSO AN EXAMPLE.

ROCK HARDNESS

VERY HARD	CANNOT BE SCRATCHED BY KNIFE OR SHARP PICK. BREAKING OF HAND SPECIMENS REQUIRES SEVERAL HARD BLOWS OF THE GEOLOGIST'S PICK.
HARD	CAN BE SCRATCHED BY KNIFE OR PICK ONLY WITH DIFFICULTY. HARD HAMMER BLOWS REQUIRED TO DETACH HAND SPECIMEN.
MODERATELY HARD	CAN BE SCRATCHED BY KNIFE OR PICK. GOUGES OR GROOVES TO 0.25 INCHES DEEP CAN BE EXCAVATED BY HARD BLOW OF A GEOLOGIST'S PICK. HAND SPECIMENS CAN BE DETACHED BY MODERATE BLOWS.
MEDIUM HARD	CAN BE GROOVED OR GOUGED 0.05 INCHES DEEP BY FIRM PRESSURE OF KNIFE OR PICK POINT. CAN BE EXCAVATED IN SMALL CHIPS TO PIECES 1 INCH MAXIMUM SIZE BY HARD BLOWS OF THE POINT OF A GEOLOGIST'S PICK.
SOFT	CAN BE GROOVED OR GOUGED READILY BY KNIFE OR PICK. CAN BE EXCAVATED IN FRAGMENTS FROM CHIPS TO SEVERAL INCHES IN SIZE BY MODERATE BLOWS OF A PICK POINT. SMALL, THIN PIECES CAN BE BROKEN BY FINGER PRESSURE.
VERY SOFT	CAN BE CARVED WITH KNIFE. CAN BE EXCAVATED READILY WITH POINT OF PICK. PIECES 1 INCH OR MORE IN THICKNESS CAN BE BROKEN BY FINGER PRESSURE. CAN BE SCRATCHED READILY BY FINGER NAIL.

FRACTURE SPACING

TERM	SPACING
VERY WIDE	MORE THAN 10 FEET
WIDE	3 TO 10 FEET
MODERATELY CLOSE	1 TO 3 FEET
CLOSE	0.16 TO 1 FOOT
VERY CLOSE	LESS THAN 0.16 FEET

BEDDING

TERM	THICKNESS
VERY THICKLY BEDDED	4 FEET
THICKLY BEDDED	1.5 - 4 FEET
THINLY BEDDED	0.16 - 1.5 FEET
VERY THINLY BEDDED	0.03 - 0.16 FEET
THICKLY LAMINATED	0.008 - 0.03 FEET
THINLY LAMINATED	< 0.008 FEET

INDURATION

FOR SEDIMENTARY ROCKS, INDURATION IS THE HARDENING OF MATERIAL BY CEMENTING, HEAT, PRESSURE, ETC.	
FRIABLE	RUBBING WITH FINGER FREES NUMEROUS GRAINS; GENTLE BLOW BY HAMMER DISINTEGRATES SAMPLE.
MODERATELY INDURATED	GRAINS CAN BE SEPARATED FROM SAMPLE WITH STEEL PROBE; BREAKS EASILY WHEN HIT WITH HAMMER.
INDURATED	GRAINS ARE DIFFICULT TO SEPARATE WITH STEEL PROBE; DIFFICULT TO BREAK WITH HAMMER.
EXTREMELY INDURATED	SHARP HAMMER BLOWS REQUIRED TO BREAK SAMPLE; SAMPLE BREAKS ACROSS GRAINS.

TERMS AND DEFINITIONS

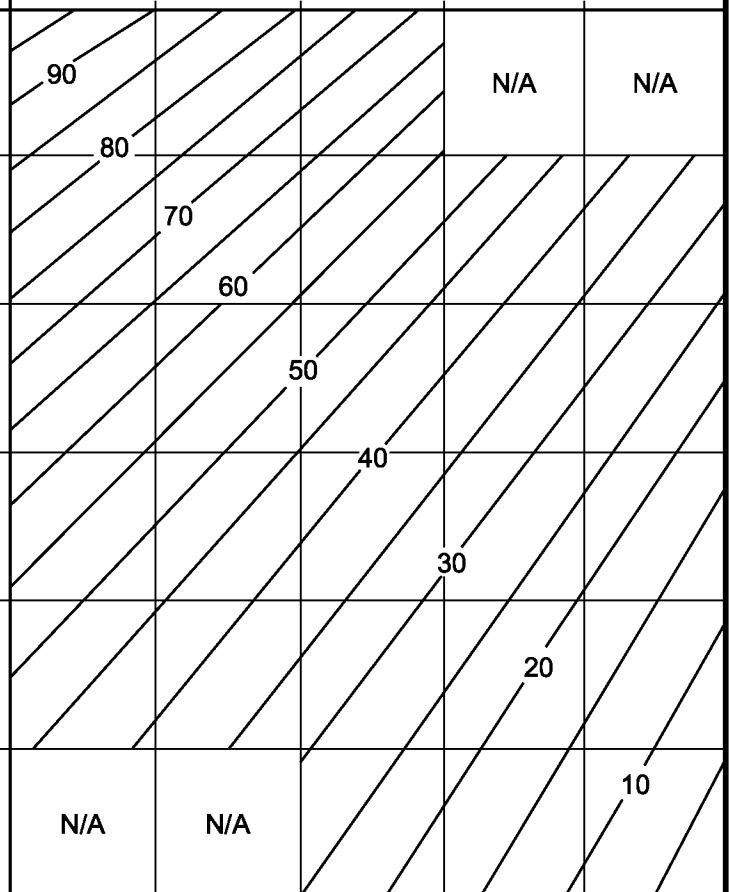
ALLUVIUM (ALLUV.) - SOILS THAT HAVE BEEN TRANSPORTED BY WATER.
AQUIFER - A WATER BEARING FORMATION OR STRATA.
ARENACEOUS - APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND.
ARGILLACEOUS - APPLIED TO ALL ROCKS OR SUBSTANCES COMPOSED OF CLAY MINERALS, OR HAVING A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, SUCH AS SHALE, SLATE, ETC.
ARTESIAN - GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL AT WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND SURFACE.
CALCAREOUS (CALC.) - SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE.
COLLUVIUM - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM OF SLOPE.
CORE RECOVERY (REC.) - TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED BY TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.
DIKE - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT ROCKS OR CUTS MASSIVE ROCK.
DIP - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE HORIZONTAL.
DIP DIRECTION (DIP AZIMUTH) - THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE LINE OF DIP, MEASURED CLOCKWISE FROM NORTH.
FAULT - A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE.
FISSILE - A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES.
FLOAT - ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLODGED FROM PARENT MATERIAL.
FLOOD PLAIN (FP) - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY THE STREAM.
FORMATION (FM) - A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN THE FIELD.
JOINT - FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED.
LEDGE - A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO ITS LATERAL EXTENT.
LENS - A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS.
MOTTLED (MOT.) - IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS. MOTTLING IN SOILS USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE.
PERCHED WATER - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE OF AN INTERVENING IMPERVIOUS STRATUM.
RESIDUAL (RES.) SOIL - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK.
ROCK QUALITY DESIGNATION (RQD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.
SAPROLITE (SAP.) - RESIDUAL SOIL THAT RETAINS THE RELIC STRUCTURE OR FABRIC OF THE PARENT ROCK.
SILL - AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, THAT HAS BEEN EMPLACED PARALLEL TO THE BEDDING OR SCHISTOSITY OF THE INTRUDED ROCKS.
SLICKENSIDE - POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT OR SLIP PLANE.
STANDARD PENETRATION TEST (PENETRATION RESISTANCE) (SPT) - NUMBER OF BLOWS IN OR BPF OF A 140 LB. HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1 FOOT INTO SOIL WITH A 2 INCH OUTSIDE DIAMETER SPLIT SPOON SAMPLER. SPT REFUSAL IS PENETRATION EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS.
STRATA CORE RECOVERY (SREC) - TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY TOTAL LENGTH OF STRATUM AND EXPRESSED AS A PERCENTAGE.
STRATA ROCK QUALITY DESIGNATION (SRQD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE.
TOPSOIL (TS.) - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.

BENCH MARK: N/A

ELEVATION: N/A FEET

NOTES:

FIAD= FILLED IMMEDIATELY AFTER DRILLING



**NORTH CAROLINA DEPARTMENT OF TRANSPORTATION
DIVISION OF HIGHWAYS
GEOTECHNICAL ENGINEERING UNIT**

SUBSURFACE INVESTIGATION

SUPPLEMENTAL LEGEND, GEOLOGICAL STRENGTH INDEX (GSI) TABLES FROM AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS (PAGE 2 OF 2)

AASHTO LRFD Figure 10.4.6.4-2 — Determination of GSI for Tectonically Deformed Heterogeneous Rock Masses (Marinos and Hoek, 2000)

GSI FOR HETEROGENEOUS ROCK MASSES SUCH AS FLYSCH (Marinos, P and Hoek E., 2000)

From a description of the lithology, structure and surface conditions (particularly of the bedding planes), choose a box in the chart. Locate the position in the box that corresponds to the condition of the discontinuities and estimate the average value of GSI from the contours. Do not attempt to be too precise. Quoting a range from 33 to 37 is more realistic than giving GSI = 35. Note that the Hoek-Brown criterion does not apply to structurally controlled failures. Where unfavourably oriented continuous weak planar discontinuities are present, these will dominate the behaviour of the rock mass. The strength of some rock masses is reduced by the presence of groundwater and this can be allowed for by a slight shift to the right in the columns for fair, poor and very poor conditions. Water pressure does not change the value of GSI and it is dealt with by using effective stress analysis.

SURFACE CONDITIONS OF
DISCONTINUITIES
(Predominantly bedding planes)

VERY GOOD - Very Rough, fresh
unweathered surfaces

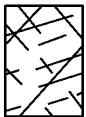
GOOD - Rough, slightly weathered
surfaces

FAIR - Smooth, moderately
weathered and altered surfaces

POOR - Very smooth, occasionally
slickensided surfaces with compact
coatings or fillings with angular
fragments

VERY POOR - Very smooth, slicken-
sided or highly weathered surfaces
with soft clay coatings or fillings

COMPOSITION AND STRUCTURE



A. Thick bedded, very blocky sandstone
The effect of pelitic coatings on the bedding planes is minimized by the confinement of the rock mass. In shallow tunnels or slopes these bedding planes may cause structurally controlled instability.



B. Sandstone with thin inter-layers of siltstone



C. Sandstone and siltstone in similar amounts



D. Siltstone or silty shale with sandstone layers



E. Weak siltstone or clayey shale with sandstone layers

C, D, E, and G - may be more or less folded than illustrated but this does not change the strength. Tectonic deformation, faulting and loss of continuity moves these categories to **F** and **H**.



F. Tectonically deformed, intensively folded/faulted, sheared clayey shale or siltstone with broken and deformed sandstone layers forming an almost chaotic structure



G. Undisturbed silty or clayey shale with or without a few very thin sandstone layers



H. Tectonically deformed silty or clayey shale forming a chaotic structure with pockets of clay. Thin layers of sandstone are transformed into small rock pieces.

Means deformation after tectonic disturbance

PROJECT REFERENCE NO.	SHEET NO.
097-01-132d4	3
SITE PLAN	
0 50 100  FEET	



SHEET 4

NC DOT BORE SINGLE SITE 097-01-132D4 WILKES COUNTY BORING LOGS.GPJ NC DOT.GDT 4/20/26

GEOTECHNICAL BORING REPORT
BORE LOG

WBS 097-01-132d4		TIP N/A		COUNTY WILKES		GEOLOGIST C. Brake												
SITE DESCRIPTION 1089 Anne-Sophia Lane for Bridge over Big Bugaboo Creek							GROUND WTR (ft)											
BORING NO. EB2		STATION N/A		OFFSET N/A		ALIGNMENT -L-		0 HR. 3.8										
COLLAR ELEV. 0.0 ft		TOTAL DEPTH 19.0 ft		NORTHING 927,131		EASTING 1,419,960		24 HR. FIAD										
DRILL RIG/HAMMER EFF./DATE F&R3763 CME-550X 89% 12/20/2024				DRILL METHOD NW Casing W/SPT & Core		HAMMER TYPE Automatic												
DRILLER S. Davis		START DATE 03/13/26		COMP. DATE 03/13/26		SURFACE WATER DEPTH N/A												
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT			SAMP. NO.	MOI	LOG	SOIL AND ROCK DESCRIPTION						
			0.5ft	0.5ft	0.5ft	0	25	50	75	100			ELEV. (ft) DEPTH (ft)					
0													0.0 GROUND SURFACE 0.0					
	0.0	0.0	2	1	2						M		ALLUVIAL Tan, Silty Fine to Coarse SAND (A-2-4) with Some Gravel					
-5	-3.5	3.5	3	4	7												-5.5 WEATHERED ROCK 5.5	
																		WEATHERED ROCK Gray MICA PHYLLITE
-10	-8.5	8.5	32	68/0.2														CRYSTALLINE ROCK 11.8
	-11.7	11.7	60/0.1										12.5					
	-14.3	14.3	60/0.0										13.6					
-15													19.0					
Notes: 1. Surficial Organic Soil= 0.0'-0.1' 2. Harder Drilling Noted by Driller at 5.5" 3. Auger Refusal at 11.7', Began Coring at 11.8'																		

GEOTECHNICAL BORING REPORT
CORE LOG

WBS 097-01-132d4				TIP N/A		COUNTY WILKES				GEOLOGIST C. Brake			
SITE DESCRIPTION 1089 Anne-Sophia Lane for Bridge over Big Bugaboo Creek										GROUND WTR (ft)			
BORING NO. EB2				STATION N/A				OFFSET N/A		ALIGNMENT -L-		0 HR. 3.8	
COLLAR ELEV. 0.0 ft				TOTAL DEPTH 19.0 ft				NORTHING 927,131		EASTING 1,419,960		24 HR. FIAD	
DRILL RIG/HAMMER EFF./DATE F&R3763 CME-550X 89% 12/20/2024								DRILL METHOD NW Casing W/SPT & Core		HAMMER TYPE Automatic			
DRILLER S. Davis				START DATE 03/13/26				COMP. DATE 03/13/26		SURFACE WATER DEPTH N/A			
CORE SIZE NQ				TOTAL RUN 7.2 ft									
ELEV (ft)	RUN ELEV (ft)	DEPTH (ft)	RUN (ft)	DRILL RATE (Min/ft)	REC. (ft) %	ROD (ft) %	SAMP. NO.	STRATA REC. (ft) %	ROD (ft) %	LOG	DESCRIPTION AND REMARKS	DEPTH (ft)	
-11.8											Begin Coring @ 11.8 ft		
	-11.8	11.8	2.5	0:29/0.5	(1.4)	(0.0)		(0.7)	(0.0)		CRISTALLINE ROCK	11.8	
	-14.3	14.3		0:39/1.0	56%	0%		100%	0%		Moderately to Severely Weathered, Hard to Medium Hard, Brown MICA	12.5	
-15			4.7	1:35/1.0							PHYLLITE with Very Close Fracture Spacing	13.6	
				N=60/0.0	(4.7)	(3.5)		(0.0)	(0.0)		WEATHERED ROCK		
				1:46/1.0	100%	74%		0%	0%		No Recovery		
	-19.0	19.0		1:50/1.0				(5.4)	(3.5)		CRISTALLINE ROCK		
				1:50/1.0				100%	65%		Moderately to Very Slightly Weathered, Hard to Medium Hard, Brown and	19.0	
				1:27/1.0							Gray MICA PHYLLITE with Very Close to Moderately Close Fracture		
				1:40/0.7							Spacing		
											Boring Terminated at Elevation -19.0 ft in CRISTALLINE ROCK (MICA		
											PHYLLITE)		
											Notes:		
											1. Surficial Organic Soil= 0.0'-0.1'		
											2. Harder Drilling Noted by Driller at 5.5"		
											3. Auger Refusal at 11.7', Began Coring at 11.8'		



CORE PHOTOGRAPH (EB2):
1089 Anne-Sophia Lane for bridge over Big Bugaboo Creek





SITE PHOTOGRAPHS:
1089 Anne-Sophia Lane for bridge over Big Bugaboo Creek



Photograph No. 1: View looking North



Photograph No. 2: View looking South



Photograph No. 3: View looking upstream



Photograph No. 4: View looking downstream



SITE ID: 097-01-7b48b

SITE ADDRESS: 167 STARLIND DR.,
MCGRADY, NC 28649

North Carolina Emergency Management – Private Roads and Bridges
Site Information Form

Site Number: 097-01-7b48b

Site Address: 167 Starline Drive, McGrady, NC 28649

GPS Coordinates: 36.3133,-81.2699

County: Wilkes

Bridge Type: Steel I-beam with Timber Decking or Modular Steel Bridge

Span Length: 40 ft Standard Bridge or 40 ft Modular Bridge. Refer to BSR for required waterway opening.

Bridge Width: 12'-0" Clear Width

Substructure Type: Concrete Cap on Drilled-in Piles

Geotechnical Information: See Standard Bridge Plans or the Modular Bridge Substructure Plans for Notes

Additional Notes: _____

Timber bridge railing not required for Steel I-beam with timber decking option.

Modular Steel Bridge option shall include guardrail as part of the system.

Wingwalls are not required.

The existing bridge is in place and must be removed by the Contractor prior to the start of construction.

No known debris or obstructions in the stream requiring removal.

BRIDGE SURVEY & HYDRAULIC DESIGN REPORT

NC DEPARTMENT OF EMERGENCY MANAGEMENT
PRIVATE ROADS AND BRIDGES PROGRAM

Site Number

097-01-7b48b

Latitude

36.31333

Longitude

-81.26981

County

Wilkes

Address

near 167 Starline Drive

City

McGrady, NC

Zip Code

28649

Recommended Structure

1 @ 40' Steel Girder Bridge with timber deck

Recommended Width of Roadway

Skew

Recommended Location is

(At) Upstream, Downstream) of Existing Crossing

Temporary Crossing



I hereby certify that that I have reviewed the existing hydraulic conveyance at this site which was a 24 ft. timber bridge with the proposed conveyance provided by the proposed 40 ft. bridge.

The proposed bridge low chord for the bridge shall be set in accordance with the the FEMA Disaster Specific Guidance for the Replacement of Private Roads and Bridges issued on 14 February 2025, "to provide bridge/culvert design plans certified (sealed, signed, and dated) by a Professional Engineer licensed in the State of North Carolina demonstrating that the newly designed and installed private bridge/culvert provides conveyance greater than or equal to the original destroyed crossing".

This certification demonstrates that the newly designed and installed private bridge/culvert provides conveyance greater than or equal to the original destroyed crossing. This is based on the best available data provided from post storm evaluations. Portions of the existing structures may have been destroyed, removed, modified or shifted from their original location or elevation.

Designed by

Assisted by

Date

6/12/2026

10:42:15 AM EDT

Seal

20646

Matthew D. Foster

Johnson, Mirmiran, & Thompson Inc.

108 Asheville Commerce Parkway

Candler, NC, 28715

License No: C-3097

Reviewed by

Date

SITE DATA

Drainage Area

Source

River Basin

Yadkin Pee-Dee

Character

Stream Classification (e.g., Trout, High Quality Water)

Class WS-II, Tr. HQW

Debris Potential: Low

☐ Moderate

☒ High

☐

Existing Structure - Source of Available Data

NCEM Private Roads and Bridges Inspection Team

Existing Structure - Description

1 @ 24 ft timber bridge

Estimated Waterway Opening

78.6

ft²

Design Control Elev

ft

Source

Gage Station No

Period of Records

Max Discharge

cfs

Date

Frequency

Historical Flood Information:

Date

Elev

ft

Est Freq

yr

Source

Period of Knowledge

yrs

Historical Scour Info: General

ft

Contraction

ft

Local

ft

Channel Slope

ft/ft

Source

Normal Water Surface Elev

ft

Manning's n: Left OB

Channel

Right OB

Source

Flood Study / Status

FEMA Study LDS (North Fork Reddies River)

Flood Study

3162

cfs

WS Elev: Floodway

1421.03

ft

Without Floodway

1421.00

ft

River Station

35034

DESIGN DATA

Hydrological Method

Disaster Specific Guidance for the Replacement of Private Roads and Bridges 2/14/2025

Hydraulic Design Method

Floods Evaluated

Frequency (year)

Discharge (cfs)

Elevation (ft)

Backwater (ft)

Bridge Opening Velocity (fps)

Waterway Opening Provided Below: Design WS Elev

sf

100-yr WS Elev

sf

Total

93.7

sf

Average Channel Velocity (Design)

fps

Average Overbank Velocity (Design)

fps

Computed Scour: General

ft

Contraction

ft

Local

ft

INFORMATION TO BE SHOWN ON PLANS

HYDRAULIC DATA

DESIGN DISCHARGE = 1710 C.F.S.

FREQUENCY OF DESIGN FLOOD = 25 YRS.

DESIGN HIGH WATER ELEVATION =

DRAINAGE AREA = 10.1 SQ. MI.

BASIC DISCHARGE (Q100) = 2570 C.F.S.

BASIC HIGH WATER ELEVATION =

OVERTOPPING FLOOD DATA

OVERTOPPING DISCHARGE = C.F.S.

FREQUENCY OF OVERTOPPING FLOOD = YRS.

OVERTOPPING FLOOD ELEVATION = *

*NOTE LOCATION OF OVERTOPPING

WS EL. Taken @ River Station ?

ADDITIONAL INFORMATION AND COMPUTATIONS

Emergency Vehicle Access Possible?	No	
Number of Homes Confirmed	No	
Number of Homes	5	
Churches Confirmed	No	
Number of Churches	0	
Schools Confirmed	No	
Number of Schools	0	
Recreational/Business Areas Confirmed	No	
Number of Recreational/Business Areas	0	
General Description	Bridge over the creek is the primary access to multiple homes on Starline Drive. It is damaged and in a state of disrepair.	
Overall Condition	Damage	
Condition Other		
Site Repair Status	Temporary Repair	
Condition Description	Damaged and in poor condition.	
Expected Level of Effort	Replace	
Other Level of Effort		
Horizontal Curve	No	
Number of Travel Lanes (LOS)	1	
Inclination	No	
Roadway Divider	No	
Road/Bridge Width (ft)	10.00	
Span/Gap Estimate (ft)	30.00	
Surface to Water (ft)	5.00	
Utility/Mechanical	No	
Utility Types		

Proposed

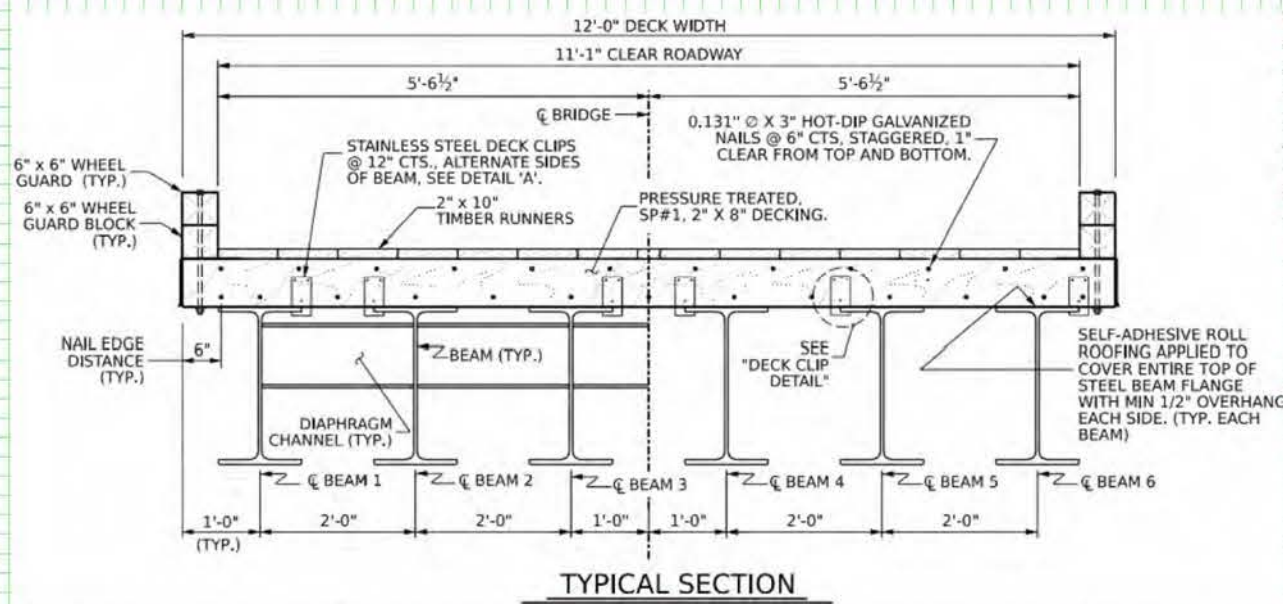
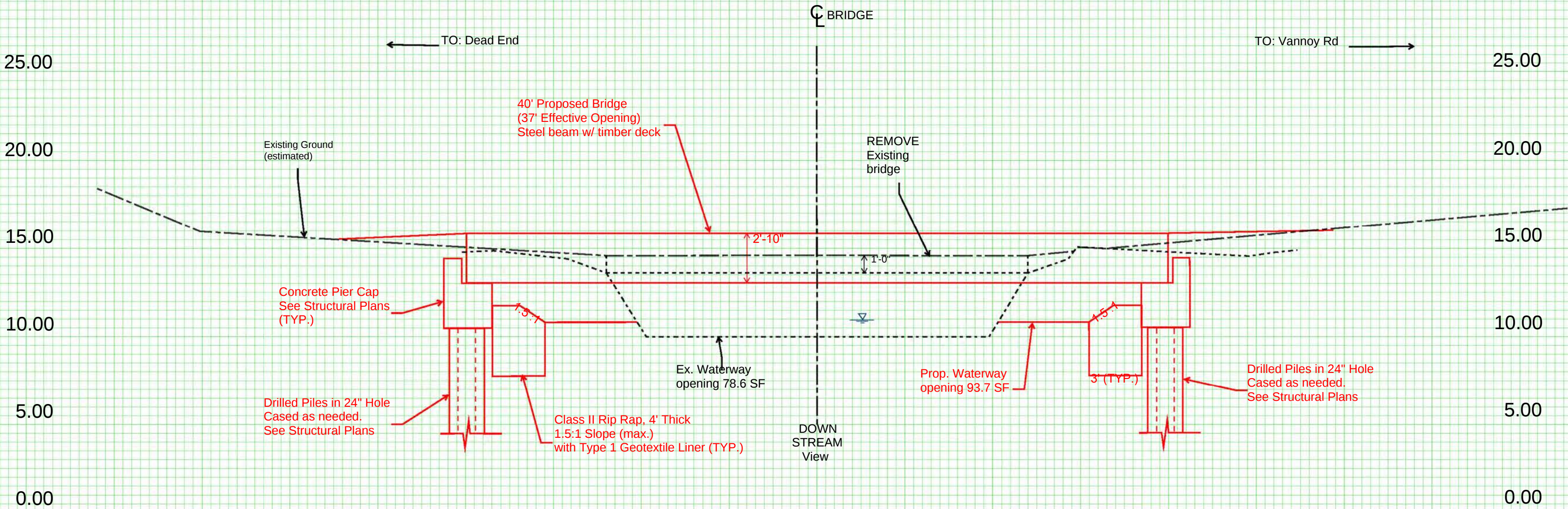
24" W24X76 beam

+ 8" Deck

+ 2" Runner

=34" (2'-10" structure depth)

10+00 10+05 10+10 10+15 10+20 10+25 10+30 10+35 10+40 10+45 10+50 10+55 10+60 10+65 10+70



Stationing and elevations shown are relative to the site.
Based on an assumed datum.
No survey grade field work was performed.

BSR based on STANDARD BRIDGE PLANS

BRIDGE SURVEY & HYDRAULIC DESIGN REPORT

NC DEPARTMENT OF EMERGENCY MANAGEMENT
PRIVATE ROADS AND BRIDGES PROGRAM

Site Number097-01-7b48bLatitude36.31333Longitude-81.26981

CountyWilkesAddressnear 167 Starline Drive

CityMcGrady, NCZip Code28649

Recommended Structure1 @ 40' Steel Modular Bridge (30' effective length)

Recommended Width of RoadwaySkew

Recommended Location is (At)Upstream, Downstream) of Existing Crossing

Temporary Crossing



I hereby certify that I have reviewed the existing hydraulic conveyance at this site which was a 24 ft. timber bridge with the proposed conveyance provided by the proposed 40 ft. bridge.

The proposed bridge low chord for the bridge shall be set in accordance with the the FEMA Disaster Specific Guidance for the Replacement of Private Roads and Bridges issued on 14 February 2025, "to provide bridge/culvert design plans certified (sealed, signed, and dated) by a Professional Engineer licensed in the State of North Carolina demonstrating that the newly designed and installed private bridge/culvert provides conveyance greater than or equal to the original destroyed crossing".

This certification demonstrates that the newly designed and installed private bridge/culvert provides conveyance greater than or equal to the original destroyed crossing. This is based on the best available data provided from post storm evaluations. Portions of the existing structures may have been destroyed, removed, modified or shifted from their original location or elevation.

Designed byAssisted by

Date6/12/202610:42:15 AM EDT

Signature of Matthew D Foster

7B1932BFAC8472..

Reviewed byDate

SITE DATA

Drainage AreaSource

River BasinYadkin Pee-DeeCharacter

Stream Classification (e.g., Trout, High Quality Water)Class WS-II, Tr. HQW

Debris Potential: LowModerateHigh

Existing Structure - Source of Available DataNCEM Private Roads and Bridges Inspection Team

Existing Structure - Description1 @ 24 ft timber bridge

Estimated Waterway Opening78.6ft²

Design Control ElevftSource

Gage Station NoPeriod of Records

Max DischargecfsDateFrequency

Historical Flood Information:

DateElevftEst FreqyrSourcePeriod of Knowledgeyrs

Historical Scour Info: GeneralftContractionftLocalft

Channel Slopeft/ftSourceNormal Water Surface Elevft

Manning's n: Left OBChannelRight OBSource

Flood Study / StatusFEMA Study LDS (North Fork Reddies River)

Flood Study100-yr Discharge3162cfsWS Elev: Floodway1421.03ftWithout Floodway1421.00ftRiver Station35034

DESIGN DATA

Hydrological MethodDisaster Specific Guidance for the Replacement of Private Roads and Bridges 2/14/2025

Hydraulic Design Method

Floods EvaluatedFrequency (year)Discharge (cfs)Elevation (ft)Backwater (ft)Bridge Opening Velocity (fps)

Waterway Opening Provided Below: Design WS Elevsf100-yr WS ElevsfTotal108.0sf

Average Channel Velocity (Design)fpsAverage Overbank Velocity (Design)fps

Computed Scour: GeneralftContractionftLocalft

INFORMATION TO BE SHOWN ON PLANS

HYDRAULIC DATA

DESIGN DISCHARGE= 1710_ C.F.S.

FREQUENCY OF DESIGN FLOOD= 25_ YRS.

DESIGN HIGH WATER ELEVATION=

DRAINAGE AREA= 10.1_ SQ. MI.

BASIC DISCHARGE (Q100)= 2570 C.F.S.

BASIC HIGH WATER ELEVATION=

OVERTOPPING FLOOD DATA

OVERTOPPING DISCHARGE= C.F.S.

FREQUENCY OF OVERTOPPING FLOOD= YRS.

OVERTOPPING FLOOD ELEVATION= *

*NOTE LOCATION OF OVERTOPPING

WS EL. Taken @ River Station ?

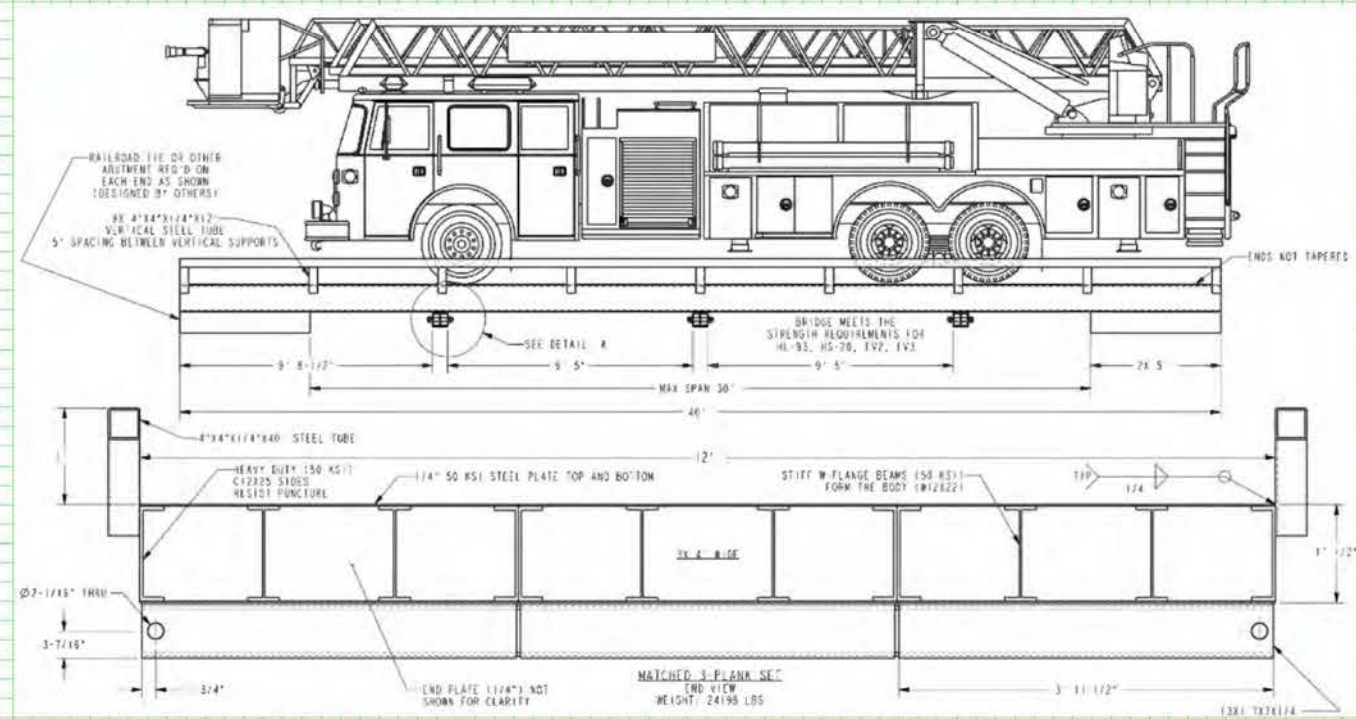
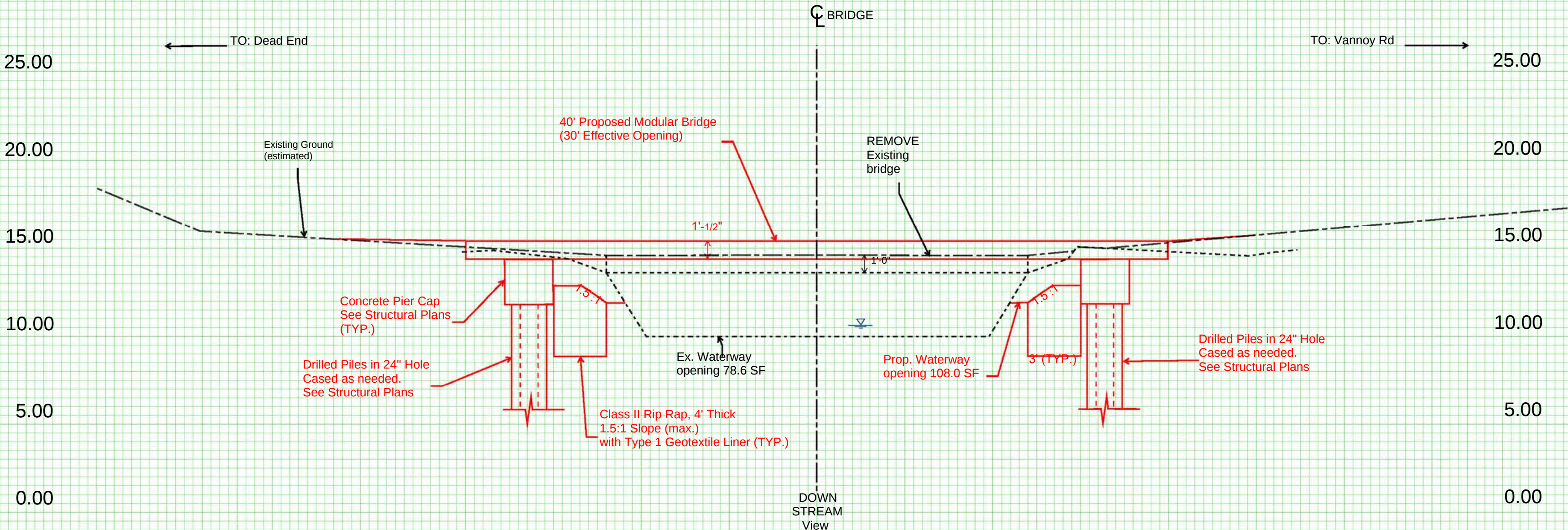
ADDITIONAL INFORMATION AND COMPUTATIONS

Emergency Vehicle Access Possible?	No
Number of Homes Confirmed	No
Number of Homes	5
Churches Confirmed	No
Number of Churches	0
Schools Confirmed	No
Number of Schools	0
Recreational/Business Areas Confirmed	No
Number of Recreational/Business Areas	0
General Description	Bridge over the creek is the primary access to multiple homes on Starlite Drive. It is damaged and in a state of disrepair.
Overall Condition	Damage
Condition Other	
Site Repair Status	Temporary Repair
Condition Description	Damaged and in poor condition.
Expected Level of Effort	Replace
Other Level of Effort	
Horizontal Curve	No
Number of Travel Lanes (LOS)	1
Inclination	No
Roadway Divider	No
Road/Bridge Width (ft)	10.00
Span/Gap Estimate (ft)	30.00
Surface to Water (ft)	5.00
Utility/Mechanical	No
Utility Types	

12" W121X22 beam
+ 0.25" Steel Plate
+ 0.25" Steel Plate
=12.5" (1'-1/2") ft structure depth)

Proposed Conveyance Area has been reduced by 0.9 sf to account for blockage created by 3 Plank Connectors as shown in Detail A of the Typical Section.

10+00 10+05 10+10 10+15 10+20 10+25 10+30 10+35 10+40 10+45 10+50 10+55 10+60 10+65 10+70



Stationing and elevations shown are relative to the site.
Based on an assumed datum.
No survey grade field work was performed.

BSR based on MODULAR BRIDGE PLANS

BORE LOG

WBS 097-01-7B48B		TIP N/A	COUNTY WILKES	GEOLOGIST J. Baskin			
SITE DESCRIPTION 167 Starline Drive for Bridge over North Fork Reddies River				GROUND WTR (ft)			
BORING NO. EB1	STATION N/A	OFFSET N/A	ALIGNMENT -L-	0 HR. NM			
COLLAR ELEV. 0.0 ft	TOTAL DEPTH 10.6 ft	NORTHING 940,623	EASTING 1,331,247	24 HR. 4.5			
DRILL RIG/HAMMER EFF./DATE F&R7348 CME-750X 87% 12/20/2024			DRILL METHOD H.S. Augers	HAMMER TYPE Automatic			
DRILLER S. Davis	START DATE 05/26/26	COMP. DATE 05/26/26	SURFACE WATER DEPTH N/A				
ELEV (ft)	DEPTH (ft)	BLOW COUNT	BLOWS PER FOOT	SAMP. NO.	LOG	SOIL AND ROCK DESCRIPTION	DEPTH (ft)
0	0.0	WOH WOH	2		M	ALLUVIAL Brown, Fine to Coarse Silty Clayey SILT (A-4) with Trace Roots and Mica Brown, Clayey Silty/Fine to Coarse SAND (A-2-4) with Trace Mica and Trace Gravel	0.0
-5	3.5	2 7 38			M		
-8.5	8.5	7 30 58			M		
-10	10.6	60/0.0			Sat.	RESIDUAL Gray, Silty Fine to Coarse SAND (A-1-b) with Rock Fragments WEATHERED ROCK Gray GRANITIC GNEISS Boring Terminated with Standard Penetration Test Refusal at Elevation -10.6 ft on CRYSTALLINE ROCK (GRANITIC GNEISS)	10.6
Note: 1. Auger Refusal at 10.6'.							

SHEET 5

DRAFT

GEOTECHNICAL BORING REPORT
CORE LOG

WBS 097-01-7B48B				TIP N/A		COUNTY WILKES				GEOLOGIST J. Baskin			
SITE DESCRIPTION 167 Starline Drive for Bridge over North Fork Reddies River										GROUND WTR (ft)			
BORING NO. EB2				STATION N/A				OFFSET N/A		ALIGNMENT -L-		0 HR. NM	
COLLAR ELEV. 0.0 ft				TOTAL DEPTH 16.2 ft				NORTHING 940,599		EASTING 1,331,282		24 HR. 3.5	
DRILL RIG/HAMMER EFF./DATE F&R7348 CME-750X 87% 12/20/2024								DRILL METHOD SPT Core Boring			HAMMER TYPE Automatic		
DRILLER S. Davis				START DATE 05/26/26				COMP. DATE 05/27/26		SURFACE WATER DEPTH N/A			
CORE SIZE NQ				TOTAL RUN 9.3 ft									
ELEV (ft)	RUN ELEV (ft)	DEPTH (ft)	RUN (ft)	DRILL RATE (Min/ft)	RUN REC. (ft) % ROD (ft) %		SAMP. NO.	STRATA REC. (ft) % ROD (ft) %		L O G	DESCRIPTION AND REMARKS		
											ELEV. (ft) DEPTH (ft)		
-6.9											Begin Coring @ 6.9 ft		
	-6.9	6.9	4.3	0:06/0.3 0:54/1.0 0:28/1.0 0:33/1.0 1:03/1.0	(2.8) 65%	(2.6) 60%		(7.6) 82%	(6.8) 73%		-6.9		
-10											CRSTALLINE ROCK		
	-11.2	11.2									Moderately Severe to Very Slightly Weathered, Moderately Hard to Hard, White-Black GRANITIC GNEISS with Very Close to Moderately Close Fracture Spacing		
			5.0	0:57/1.0 0:35/1.0 0:52/1.0 1:01/1.0 1:26/1.0	(4.8) 96%	(4.2) 84%							
-15													
	-16.2	16.2									-16.2		
Boring Terminated at Elevation -16.2 ft in CRYSTALLINE ROCK (GRANITIC GNEISS)													
Note: 1. Auger Refusal at 6.8'. Begin Coring at 6.9'.													

DRAFT